### AVIONICS SYSTEMS ENGINEERING DIVISION

(NASA-CR-140 '58) RCS PROPULSION

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RCS PROFULSION FUNCTIONAL PATH ANALYSIS FOR PERFORMANCE MONITORING FAULT DETECTION

AND

**ANNUNCIATION** 

DISTRIBUTION AND REFERENCING



National Aeronautics and Space Administration LYNDON B. JOHNSON SPACE CENTER

Houston, Texas

July 1974

LEC-3594

### AVIONICS SYSTEMS ENGINEERING DIVISION

RCS PROPULSION FUNCTIONAL PATH AMALYSIS FOR PERFORMANCE MONITORING FAULT DETECTION AND ANNUNCIATION

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### **ABBREVIATIONS**

Aux Auxiliary

Eng Engine

FCS Flight Control System

Fu Fuel

Fwd Forward

He Helium

Injr Injector

Isln Isolation

L Left

Manf Manifold

OMS Orbital Maneuvering System

Ox or Oxid Oxidizer

Pos Position

Prplt Propellant

R Right

RCS Reaction Control System

Rlf Relief

Rgltr Regulator

SOV Shut-off valve

Temp Temperature

Tk Tank

XFD Crossfeed

### 1.0 SUMMARY

The Reaction Control System (RCS) is not completely defined at this time. The configuration considered in this document is shown in the illustrations included in this document.

Future configuration changes should have little impact on the measurements required for fault detection and annunciation.

One hundred and eleven measurements have been identified for use in fault detection and annunciation, that are not included in the Master Measurements List, dated November 16, 1973.

These measurements are divided into the following categories:

•	Burn through monitors	44	ea
•	Engine temperatures	4	ea
•	Manifold pressures	30	ea
•	Shut-off valve positions	22	ea
•	Redundant helium source pressures	9	ea
•	Cargo bay tank pressures	2	ea

Consideration should be given to including the following in the design of the reaction jet drivers:

• Redundant chamber pressure sensors.

- Jet driver output monitors.
- Jet driver electrical-ON failure isolation capability.
- Single jet driver power isolation capability.
- Failure identification annunciation.

### 2.0 INTRODUCTION

### 2.1 Purpose

This document defines the functional paths of the RCS and defines the operational flight instrumentation required for performance monitoring fault detection and annunciation.

A functional path, as used in this document, is defined as one or more functional elements which may be combined into operating functional paths which are controllable or selectable by the flight crew for systems management.

### 2.2 System Description

2.2.1 Reaction Control System (RCS). The RCS, operating in conjunction with the Guidance Navigation and Control Subsystem, employs 38 bipropellant primary and six vernier thrusters to provide precise attitude control and three-axis translation during separation from the external tank, orbit insertion, orbital and recently phases of flight.

In addition, the RCS provides roll control during single engine orbital maneuvering system burns.

2.2.2 RCS organization. The RCS consists of three independent propulsion packages. One module, comprising 14 primary thrusters and two verniers, is located in the forward fuselage and the other two modules, each containing 12 primary thrusters and two vernier thrusters, are contained in the auxiliary propulsion subsystem mounted on each side of the aft fuselage.

- 2.2.3 RCS components. Each RCS Propulsion Package contains a propellant storage and distribution system, a helium pressurant gas storage regulation and distribution system, a thermal control assembly, and electrical and flight instrumentation system. Each primary thruster produces approximately 900 pounds thrust. The vernier thrusters provide approximately 25 pounds thrust each.
- 2.2.4 RCS propellant supply. The hypergolic RCS propellants are nitrogen tetroxide  $(N_2O_4)$  and monomethalhydrazine. Each RCS is normally supplied propellants from its own dedicated set of tanks. Crossfeed lines provide the capability to supply propellant to either aft RCS thrusters from one of the following sources:
  - OMS propellant tanks
  - Cargo bay kit tanks
  - Pod tanks from the opposite RCS
- 2.2.5 RCS activation. During liftoff and ascent, the RCS is inactive with the helium isolation valves closed and the propellant isolated from the thruster bipropellant valve inlets by the propellant isolation valves. Prior to external tank jettison, the propellant isolation valves, the helium isolation valves, and the RCS doors are commanded open and the RCS propellant and pressurization subsystems are ready for operation
- 2.2.6 RCS reentry configuration. The forward RCS is not used during reentry. Prior to reentry, the forward RCS jets are deactivated, and the RCS doors are closed.

- 2.2.7 Failed thruster monitoring. Guidance and control will monitor for failed thrusters. It is assumed that a fault word will be provided from the guidance and control computer for performance monitoring fault annunciation.
- 2.2.8 RCS configuration status. Several areas of the RCS are not defined at this time. For the purpose of this report, these areas are assumed to be as shown on the system prints in this document.

Vernier jet location and manifold connections, RCS door instrumentation, and the guidance and control monitors are likely change points.

### 3.0 FUNCTIONAL PATH ANALYSIS OF THE FORWARD RCS

### 3.1 Functional Path Identification

The functional paths for the forward RCS are identified as RCXX on figures 1 through 3.

### 3.2 Functional Path Description

RC1 is the helium source bottle for supplying helium pressure to the fuel tank. The bottle has a volume of approximately 2.02 cubic feet and is pressurized to 3600 psia prior to liftoff. RC2 provides the same function for the oxidizer tank.

RC3 through RC6 are helium isolation valves in series with two helium regulators. They provide helium source isolation and regulate source pressure to a propellant tank pressure of approximately 280 psia.

RC7 and RC8 are series parallel check valves that isolate propellant from the helium regulators.

RC9 and RC10 provide over pressure relief for the fuel and oxidizer tanks. They consist of a normally open shut-off valve (SOV) in series with a burst disc and a poppet relief valve. Over pressure will rupture the burst disc allowing excess helium to be vented. In the event the poppet valve fails to reseat, the SOV is closed by the crew.

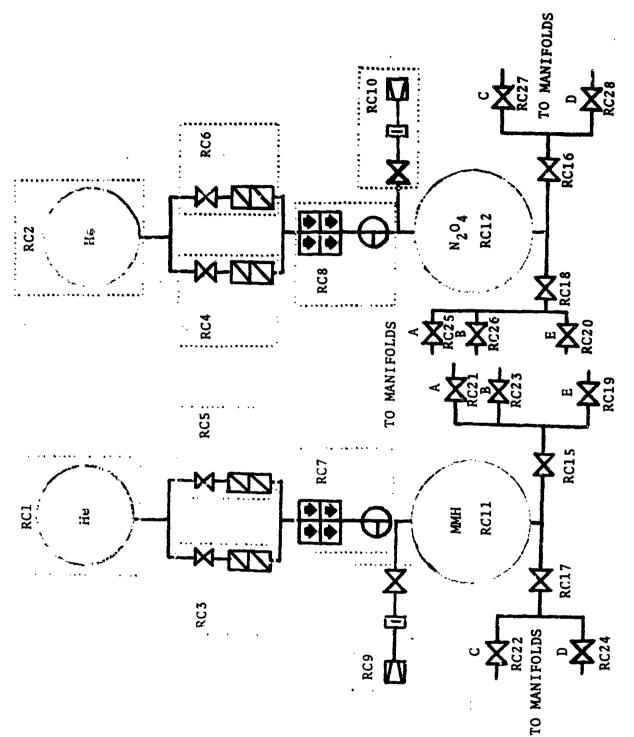


Figure 1. - Forward RCS propellant supply functional paths.

RC57 RC55 RC53 RC51 RC49 RC47 RC45 RC43 RC41 RC39 RC37 RC35 TO MANIFOLD ISOLATION VALVES RC33 RC31 RC29 ပ ŏ FUEL

RC59

- Functional paths forward RCS A and C manifold thrusters. Figure 2.

RC60 RC58 RC56 RC54 RC48 RC46 RC44 RC42 RC40 RC38 RC32 RC30 χo RC64 ш RC62 RC63 FUEL RC61 Щ

TO MANIFOLD ISOLATION VALVES

Figure 3. - Functional paths forward RCS E, B, and D manifolds.

RC11 and RC12 are propellant holding tanks. Each tank has a volume of approximately 14 cubic feet.

RC15 through RC18 are tank isolation valves used to isolate propellant flow from the propellant tanks to the manifold isolation valves.

RC19 through RC28 are manifold isolation valves. Each valve controls the flow of fuel or oxidizer to the inlet of four primary or two vernier jets. In the event of a failed-on thruster or a leak, both the fuel and oxidizer ranifold isolation valves associated with the failure are closed.

RC29 through RC64 are engine inlet valves for fuel and oxidizer. Each engine has a dedicated jet driver which opens and closes the fuel and oxidizer inlet valves on command.

### 3.3 Operating Functional Paths

Functional paths are combined into operating functional paths for fault detection and annuaciation. The operating functional paths are identified as ORCXX. A total of 16 fuel and 16 oxidizer functional paths exist in the forward RCS system.

All functional paths for fuel are identical from the helium source to the fuel tank isolation valves.

ORC1 = (RC1) (RC3 + RC5) (RC7) (RC11)

In addition, two sets of eight engines have a common path through the fuel tank isolation valves.

ORC2 = (ORC1) (RC15)

ORC3 = (ORC1) (RC17)

Five groups of engines have common fuel paths through the manifold isolation valves.

ORC4 = (ORC2) (RC21) for Manifold A

ORC5 = (ORC3) (RC22) for Manifold C

ORC6 = (ORC2) (RC23) for Manifold B

ORC7 = (ORC3) (RC24) for Manifold D

ORC8 = (ORC2) (RC19) for Manifold E

The complete fuel flow path for each engine is the manifold path combined with the engine inlet. The fuel flow paths for the engines are:

ORC9 = (ORC4) (RC41)for Jet 1 ORC10 = (ORC4) (RC49)for Jet 5 ORC11 = (ORC4) (RC33)for Jet 9 for Jet 13 ORC12 = (ORC4) (RC57)for Jet 3  $ORC13 \approx (ORC5) (RC37)$ ORC14 = (ORC5) (RC45)for Jet 7 for Jet 11 ORC15 = (ORC5) (RC29)ORC16 = (ORC5) (RC53)for Jet 15 ORC18 = (ORC6) (RC42)for Jet 6 ORC19 = (ORC6) (RC58)for Jet 10 ORC21 = (ORC7) (RC46)for Jet 4

ORC22 = (OPC7) (RC38) for Jet  $^{9}$ 

ORC23 = (ORC7) (RC54) for Jet 12

ORC24 = (ORC7) (RC30) for Jet 16

ORC51 = (ORC8) (RC61) for Jet 101

ORC52 = (ORC8) (RC62) for Jet 102

Oxidizer flow paths are similar and compiled as follows:

### • Common Path to Tank Isolation Valves

ORC25 = (RC2) (RC4 + RC6) (RC8) (RC12)

### • Common Paths through Tank Isolation valves

ORC26 = (ORC25) (RC18)

ORC27 = (ORC25) (RC16)

### • Common Paths to Manifolds

ORC28 = (ORC26) (RC25) A Manifold

ORC29 = (ORC27) (RC27) C Manifold

ORC30 = (ORC26) (RC26) B Manifold

ORC31 = (ORC27) (RC28) D Manifold

ORC32 = (ORC26) (RC20) E Manifold

### • Oxidizer Flow Paths to Jet:

ORC33 = (ORC28) (RC43) for Jet 1

ORC34 = (ORC28) (RC51) for Jet 5

ORC35 = (ORC28) (RC35) for Jet 9

ORC36 = (ORC28) (RC59) for Jet 13

ORC37 = (ORC29) (RC39) for Jet 3

ORC38 = (ORC29) (RC47) for Jet 7

ORC39	*	(ORC29)	(RC31)	for	Jet	11
ORC40	=	(ORC29)	(RC55)	for	Jet	15
ORC42	=	(ORC30)	(RC44)	for	Jet	6
ORC43	=	(ORC30)	(RC60)	for	Jet	10
ORC45	*	(ORC31)	(RC48)	for	Jet	4
ORC46	=	(ORC31)	(RC40)	for	Jet	8
ORC47	=	(ORC31)	(RC56)	for	Jet	12
ORC48	=	(ORC31)	(RC32)	for	Jet	16
ORC49	=	(ORC32)	(RC63)	for	Jet	101
ORC50	=	(ORC32)	(RC64)	for	Tet	102

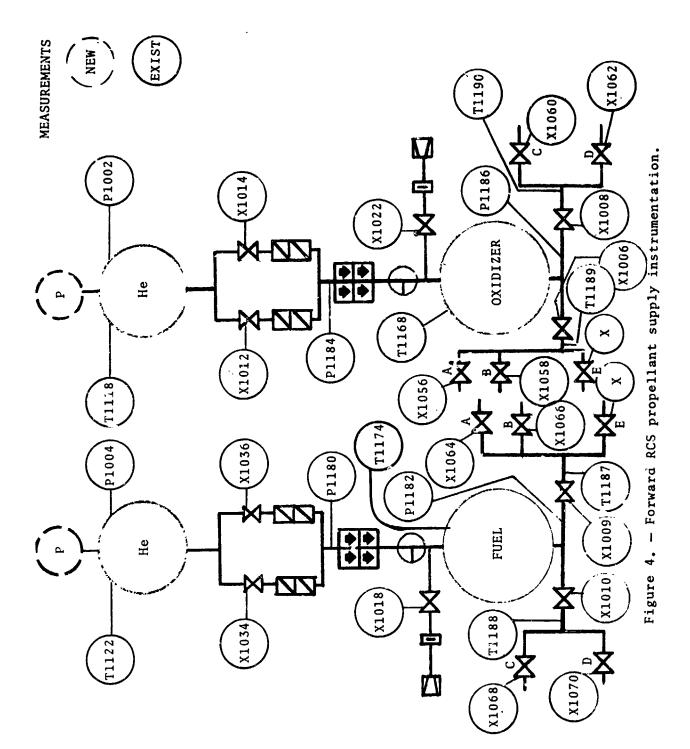
## 4.0 MEASUREMENT REQUIREMENTS FOR FAULT DETECTION AND ANNUNCIATION - FORWARD RCS

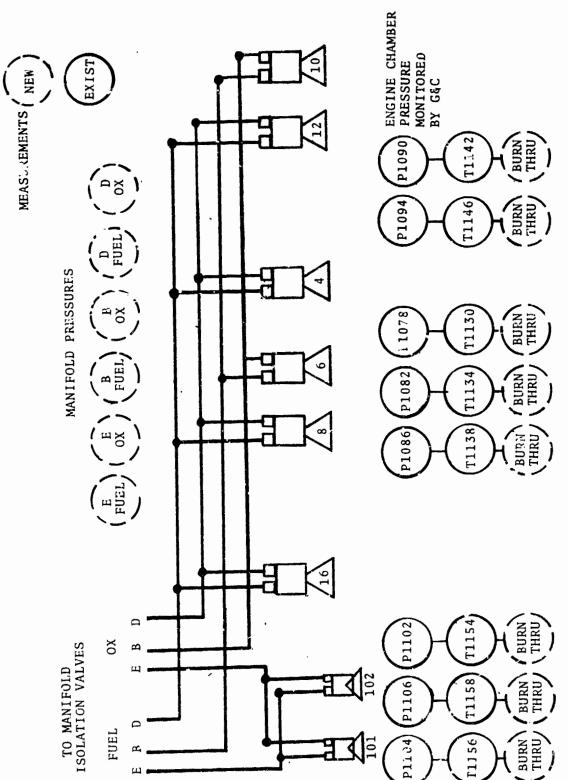
### 4.1 FDA Measurements

Table 1 lists the primary, correlation, and preconditioning measurements required for fault detection and annunciation. The table identifies 28 new measurements not included in the Master Measurements List, dated November 16, 1973. Measurement justification is also included in table 1. Figures 4 through 6 show the approximate location of the forward RCS measurements.

- 4.2 Description of Parameters to be Monitored
- 4.2.1 Helium source pressure. Helium source pressure is used for propellant gauging and is the best overall indicator of system integrity. In the event the source pressure measurement is lost, the system status and propellant remaining cannot be determined; therefore, redundant source pressure measurements should be added.
- 4.2.2 <u>Propellant pressures</u>. Helium SOV positions provide a precondition check to determine if the system is static or dynamic. Regulator output is required to isolate leaks and failed components such as regulators, helium SOV's, and vent valves.

Tank outlet pressure provides a correlation check for regulator output pressure.





Figu 9 5. - Forward manifolds B, D, and E instrumentation.

Figure 6. - Forward manifolds A and C instrumentation.

1-4

4.2.3 <u>Manifold pressures</u>. Tank outlet SOV's and manifold isolation valves provide precondition checks for manifold pressure checks.

Manifold pressure transducers should be added to provide rapid leak isolation capabilities. Heat soak back monitoring for failed manifolds would also be provided by these transducers.

4.2.4 <u>Thruster temperature</u>. Thruster temperature transducers should be monitored for overtemperature during burns and for leak indications during quiescent periods.

In addition, the engine procurement specification provides for burn-through monitors on each engine. It is anticipated that they will be monitored by PMS.

### 4.3 Leak Detection Methods

- 4.3.1 Quantity remaining. Premission helium profiles are not adequate for helium monitoring. Leaks can be detected by correlating helium source pressure with quantity of propellant remaining. Since quantity remaining is gauged by helium pressure, volume, and temperature, quantity measurements become inaccurate when a leak is introduced into the system. A thruster-on time multiplied by flow rate calculation should be correlated with quantity remaining.
- 4.3.2 <u>Delta pressure</u>. The helium source pressure delta for fuel and oxidizer should be nearly constant, since equal volumes of fuel and oxidizer are being consumed. A change in the delta pressure is indicative of a leak.

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TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD RCS FAULT

## DETECTION AND ANNUNCIATION

N + m +	าร			<b>1</b> -	Z						60		F	<b>b</b> 0	_		
Justification		System status and	leak monitor	System status lost	Should be	redundant	Heat and cold	soak, Leak	monitor.	Position defines	type of monitoring	static or dynamic	Position defines	type of menitoring	static or	dynamic	**N = New Measurement Required
Operating functional	patn	RC1	ORC1	171	RC1	TOWN	1	RCI	ORC1	ļ	RC3	ORC1		ORC I	RC 5		w Measurem
oft limit Hard limit Correlation	measurement	T1120A	T1122A		T1120A			NA			AN			N.A			**N " Ne
limit	MOT	llant	dent	llant	ning	dent		TBD			AN			AN		7	
Hard	nıgn	Propellant remaining	dependent	Propellant	remaining	dependent		ŢBD			NA			NNA			
limit	MOT	X.			N A			TBD			NA			AN			
Soft	nıgn	Z A	,		Y N			TBD			ΝA			NA			
<b>*</b> ⊃ o o	υ	Δ.			۵,			၁			×			×		J	<u>خ</u>
Measurement		N (3)	tk press	RCS fwd	He fuel	}	7	He fuel		X1034	KCS IWG He		V42X1036E	FCS ING HE	۲ ک	7 DATEA HTST	*F = Primary

C \* Correlation

X = Precondition

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD RCS FAULT

# DETECTION AND ANNUNCIATION - Continued

Status						
Justification	System status and leak and over- pressurization monitor		Heat and cold soak. Leak detection.	Note: Measurement No. may change on new configuration	Heat soakback	Heat soakback
Operating functional path	ORC 1	ORC 1	ORC 1 RC11	RC17 ORC2	ORC2	ORC3
limit Correlation low measurement	P1182A T1172A T1174A	NA	NA			
limit low	275 psig	275 psig	ТВD	NA	TBD	ТВD
Hard High	300 psig	300 psig	TBD	NA	TBD	ТВD
oft limit igh low	ТВД	NA	ТВD	NA	TBD	ТВD
Soft High	ТВД	NA	ТВD	NA	твр	ТВD
e s C*	ď	C	P	×	ď	д
Measurement	V42P1180A RCS fwd fu RGLTR out press	V42P1182A RCS fwd fu propellant manf press	V42T1172A RCS fwd fu storage tank shell temp	V42X1009E RCS fwd fu tank shut- off valve 1	V42T1187A RCS fwd fu manifold temp No 1	V42TI188A RCS fwd fu manifold temp No 2

TABLE 1..- MEASUREMENTS REQUIRED FOR FORWARD RCS FAULT
DETECTION AND ANNUNCIATION - Continued

s t s					Z	Z	Z	Z
Justification	Isolated manifold monitur	Isolated manifold monitor	Isolated manifold monitor	Isol.ted manifold monitor	Leak isolation heat soakback		Leak isolation heat soakback	Leak isolation heat soakback
Operatin; functional path	RC21 ORC4	ORC6 RC23	RC22 ORC6	RC24 ORC7	ORC4	ORC6	ORCS	ORC7
Correlation measurement			NA	NA	P1182A	P1182A	P1182A	P1182A
ft limit Hard limit gh low High low	NA	NA	NA	NA	TBD	ТВD	TBD	TBD
Hard High	NA	NA	NA	NA	TBD	TBD	TBD	TBD
limit low	NA	NA	NA	NA	NA	NA	NA	NA
Soft	NA	NA	VΝ	NA	NA	ΑN	AN	NA
#⊃ v e	۵.	م	P-	F	<u>a</u>	<u> </u>	<del>  =</del> -	Α.
Measurement	V42X1064E RCS fwd fu thruster Isln valve A	V42X1068E RCS fwd fu thruster Isln valve C	V47X1066E RCS fwd fu thruster Isln valve B	V42X1070E RCS fwd fu thruster Ísln valve D	A manifold fu press	B manifold fu press	C manifold fu press	D manifold fu press

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD RCS FAULT
DETECTION AND ANNUNCIATION - Continued

Nhah	าร			J	Z		L			<b>be</b> -							
Justification		System status	leak monitoring	System status lost	if Pl002A fails.	redundant	Heat and cold soak	leak monitor	Position defines	type of monitoring	dynamic	Position defines	type of monitoring	static or dvnamic	System status	leak and over-	pressurization monitoring
Operating functional	path	RC2	ORC25			ORC25	RC2	ORC25		KC4	ORC25		KC6	OR:225		ORC25	
oft limit Hard limit Correlation	measurement	T1116A			T1116A		42			NA			NA			P1186A	
limit	low	Propellant remaining	dependent	<b>Propellant</b>	remaining	dependent	TRD	)		NA			NA			275	psig
Hard	High	Prop rema	depe	Prop	rema	depe	חאיר	1		NA			NA			300	psig
limit	low	NA			NA		TRD	1		NA			NA			275	psig
	High	NA			NA		TRD			NA			NA			282	psig
«n Q	ø	Ъ			Ы		J			×			×			b	
Measurement		V42P1002A RCS fwd He	oxid tk press	RCS fwd	He oxid	tk press	,\$	oxdzr tank temp No 1	V42X1012E	RG E	ŀ	1014	KCS IWG DE		P 1	+	oxid Kulik out press

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD RCS FAULT
DETECTION AND ANNUNCIATION - Continued

S t d b t b s		L	0.11	0.41	
Justification	Tank pressure monitor if reg pressure trans-ducer fails	Heat and cold soak leak detection	Determine tank use Note: Measurement No. may change on new configuration	Determine tank use Note: Measurement No. may change on new configuration	Heat soakback
Operating functional path	ORC25	RC12 ORC25	RC18 ORC25	RC16 ORC25	0RC26
oft limit Hard limit Correlation ligh low High low measurement	NA	NA	NA	NA	NA
limit low	275 psig	ТВD	NA	NA	ТВD
Hard High	300 psig	ТВD	NA	NA	ТВО
limit low	NA	TBD	NA	NA	TBD
Soft ] High	NA	ТВD	NA	NA	TBD
s e e	C	Ъ	×	×	Ъ
ੜ	V42P1186A RCS fwd oxid propellant manf press	V42T1168A RCS fwd oxid stor tank shell temp	V42X1006E RCS fwd oxid tank shut- off val/e No 1	V42X1008E RCS fwd oxid tank shut- off valve No 2	V4ZTI189A RCS fwd oxid manifold temp No 1

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD RCS FAULT
DETECTION AND ANNUNCIATION - Continued

0) 42 (0 42 5)	<u> </u>		L	<u> </u>		
Justification	Heat soakback	Isolated manifold monitor	Isolated manifold monitor	Isolated manifold monitor	Isolated manifold monitor	Leak isolation heat soakback
Operating functional path	ORC27	RC25 ORC28	RC27 ORC29	RC26 ORC30	RC28 ORC31	ORC28
Correlation measurement	NA	NA	NA	NA	NA	P1186A
limit low	TBD	NA	NA	NA	NA	TBD
Hard High	ТВD	NA	NA	NA	NA	TBD
limit low	ТВD	NA	NA	NA	NA	NA
Soft	TBD	NA	NA	NA	NA	NA
*⊃ s o	Д	<u> </u>		d		<u>C,</u>
Measurement	V42T1190A RCS fwd oxid manifold temp No 2	V42X1056E RCS fwd oxid thruster Isln valve A	V42X1060E RCS fwd oxid thruster Isln valve C	V42X1058E RCS fwd oxid thruster Isln valve B		RCS fwd A manifold oxid press

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD FAULT
DETECTION AND ANNUNCIATION - Continued

	*⊅	Soft	limit	Hard	limit	ft limit Hard limit Correlation	Operating	T	a t ss
Measurement	o o	High	low	High	10%	measurement	path	ממי ביו ורפרוסיי	<b>5</b> 2 4
RCS fwd B manifold oxid press	Ъ	NA	NA	TBD	ТВД	P1186A	ORC30	Leak isolation heat soakback	Z
RCS fwd C manifold oxid press	<u>a</u>	NA	NA	ТВО	TBD	P1186A	ORC29	Leak isolation heat soakback	Z
RCS fwd D manifold oxid press	Д	NA	NA	TBD	ТВD	P1186A	ORC31	Leak isolation heat soakback	Z
V42T1124A RCS fwd   p   thruster injn   temp No 1	1 P	TBD	TBD	ТВД	TBD	NA	ORC4 ORC33 Jet 1	Overtemp and leak monitor	
V42T1128A RCS fwd Pthruster injntemp No 3	d	ТВD	ТВD	TBD	ТВD	NA	ORCS ORC37 Jet 3	Temp and leak monitor	
V42T1132A RCS fwd pthruster injn temp No 5	_ <sup>ഫ</sup> പ്പ _	TBD	TBD	TBD	ТВD	NA	ORCIO ORC34 Jet 5	Temp and leak monitor	
V42TII36A RCS fwd p thruster injn temp No 7	e	TBD	TBD	TBD	ТВД	NA	ORC14 ORC38 Jet 7	Temp and leak monitor	

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD FAULT

# DETECTION AND ANNUNCIATION - Continued

statas	<b></b>					
Justification	Temp and leak monitor	Temp and leak monitor	Temp and leak monitor	Temp and leak monitor	Overtemp and leak monitor	Overtemp and leak monitor
Operating functional path	ORC11 ORC35 Jet 9	ORC15 ORC39 Jet 11	ORC12 ORC36 Jet 13	ORC16 ORC40 Jet 15	0RC21 0RC45 Jet 4	ORC18 ORC42 Jet 6
Soft limit Hard limit Correlation High low High low measurement	NA	NA	NA	NA	NA	NA
limit low	ТВD	ТВD	TBD	ТВD	ТВD	ТВD
Hard High	TBD	TBD	ТВD	TBD	TBD	TBD
limit low	ТВD	ТВЭ	ТВD	ТВD	ТВD	ТВD
Soft High	TBD	TBD	TBD	ТВD	ТВЛ	ТВD
es C*	<u> </u>	<u> </u>	ם	<u> </u>	<u> </u>	<u> </u>
Measurement	V42T1139A RCS fwd thruster injr temp No 9	V42T1144A RCS fwd thruster injr temp No 11	V42T1148A RCS fwd thruster injn temp No 13	V42T1152A RCS fwd thruster injn temp No 15	V42T1130A RCS fwd thruster injn temp No 4	V42T1134A RCS fwd thruster injn temp No 6

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD FAULT
DETECTION AND ANNUNCIATION - Continued

s ב ד a ר S	1		1	1	<u> </u>	
,,,, .,	<del> </del>	<del></del>				
Justification	Overtemp and leak monitor	Overtemp and leak monitor	Overtemp and leak monitor	Overtemp and leak monitor	Overtemp and leak monitor. Note: Injn No may change	ORC52 Overtemp and ORC50 leak monitor. Note: Injn No Jet 101 may change
Operating functional path	ORC22 ORC46 Jet 8	ORC19 ORC43 Jet 10	ORC23 ORC47 Jet 12	ORC24 ORC48 Jet 16	ORC51 ORC49 Jet 101	ORC52 ORC50 Jet 101
Soft limit Hard limit Correlation High low High low measurement	NA	NA	NA	NA	NA	NA
limit low	TBD	ТВD	TBD	TBD	ТВD	TBD
Hard High	TBD	TBD	ТВД	TBD	TBD	TBD
limit low	TBD	ТВD	ТВО	ТВD	ТВD	ТВD
	ТВD	ТВD	TBD	ТВD	TBD	ТВр
*D % 0	<u> </u>	<u> </u>	~~~	4-	<u> </u>	<u> </u>
Measurement	V42T1138A RCS fwd thruster injn temp No 8	V42T1142A RCS fwd thruster injn temp No 10	V42T1146A RCS fwd thruster injn temp No 12	V42T1154A RCS fwd thruster injn temp No 16	V42T1156A RCS fwd thruster injn temp No i01	V42T1158A RCS fwd thruster injn temp No 102

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD FAULT
DETECTION AND ANNUNCIATION - Continued

tS	<b>8</b>	Z	Z	Z	Z	Z	Z	Z	Z
	Jus <sup>+:</sup> fication	Safety monitor	Safety monitor	Safety monitor					
Operating	functional path	ORC9 ORC33 Jet 1	ORC13 ORC37 Jet 3	ORC10 ORC34 Jet 5	ORC14 ORC38 Jet 7	ORCII ORC35 Jet 9	ORCIS ORC39 Jet 11	ORC12 ORC36 Jet 13	ORC16 ORC40 Jet 15
Correlation	measurement	NA	NA	NA	NA	NA	NA	NA	NA
limit	Tow	NA	NA	NA	ŇA	NA	NA	NA	NA
Hard	High	NA	NA	NA	NA	NA	NA	NA	NA
limit	low	NA	NA	NA	NA	NA	NA	NA	NA
Soft	High	NA	NA	NA	NA	NA	NA	NA	NA
*	o s o	급	급	гЪ	n P	- <del>L</del>	H	nP	<del>П</del> -
	Measurement	RCS fwl thruster burnP thru No 1	RCS fwd thruster burnP thru No 3	RCS fwd thruster burnP thru No 5	RCS fwd thruster burnP thru No 7	RCS fwd thruster burnP thru No 9	RCS fwd thruster burnP thru No 11	RCS fwd thruster burnP thru No 13	RCS fwd thruster bu <i>r</i> nP thru No 15

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD FAULT

# DETECTION AND ANNUNCIATION - Continued

s + s	s C	Z	Z	z	Z	Z	Z	Z	Z
Tue tification	ממפרונומו	Safety monitor	Safety monitor	Safety monitor	Safety monito.	Safety moritor	Safety monitor	Safety monitor	Safety monitor
Operating	path	ORC21 ORC45 Jet 4	ORC18 ORC42 Jet 6	ORC22 ORC46 Jet 8	ORC19 ORC43 Jet 10	ORC23 ORC47 Jei 12	ORC24 ORC48 Jet 16	ORC49 ORC51 Jet 101	ORCSO ORCS2 Jet 102
Correlation	measurement	NA	NA	NA	NA	NA	NA	NA	NA
	low	NA	NA	NA	ŇA	NA	NA	NA	NA
Hard limit	High	NA	NA	NA	NA	NA	NA	NA	NA
limit	low	NA	NA	NA	NA	NA	NA	NA	NA
Soft	High	NA	NA	NA	NA	NA	ÑА	NA	NA
*>	,	пР	H P	<del>- 2</del> -	2	밑	<u> </u>	<u> </u>	<u> </u>
Measurement		RCS fwd thruster burnP thru No 4	RCS fwd thruster burnP thru No 6	RCS fwd thruster burnP thru No 8	RCS fwd thruster burnP thru No 10	RCS fwd thruster burnP thru No 12	RCS fwd thruster burnP thru No 16	RCS fwd thruster burn thru No 101	RCSfwd thruster burnP thru No 102

TABLE 1.- MEASUREMENTS REQUIRED FOR FORWARD FAULT
DETECTION AND ANNUNCIATION - Concluded

ĺ									
Measurement		Soft	limit	Hard	limit	ft limit Hard limit Correlation	Operating functional	Justification	4 b t v
	s o	High	low	High	10w	measurement	path		n
E manifold fuel press	e,	NA	NA	TBD	TBD	NA	ORC8	Leak isolation	Z
manifold oxid press	<u>a</u>	NA	NA	TBD	TBD	NA	ORC32	Leak isolation	Z
V42X1052E E manifold f Isln valve position	fup	NA	NA	NA	NA	NA	ORC8	Failed manifold monitor	
! ^	XO T	NA	NA	NA	NA	NA	ORC32	Failed manifold monitor	
V42X1018 vent valve SCV	Ъ	NA	NA	NA	NA	NA	RC9	Safety	
V42X1022 vent valve SOV	<u>a</u>	NA	NA	NA	NA	NA	RC10	Safety	

# 5.0 FUNCTIONAL PATH ANALYSIS OF THE AFT RCS

### 5.1 Functional Path Identification

The functional paths for the aft RCS are identified as RCXX on figures 7 through 10.

# 5.2 Functional Path Description - Aft Left RCS

RC70 is the helium source bottle for supplying helium pressure to the fuel tank. The bottle has 2.02 cubic feet volume and is pressurized to 3600 psia prior to liftoff.

RC71 provides the same function for the oxidizer tanks.

RC72 through RC75 are helium isolation valves in series with two helium regulators. They provide helium isolation and regulate source pressure to a propellant tank pressure of approximately 280 psia.

RC76 and RC77 are series parallel check valves that isolate propellants from the helium regulators.

RC80 and RC81 provide over pressure relief for the fuel and oxidizer tanks. They consist of a normally open 50V in series with a burst disc and a poppet relief valve. Over pressure will rupture the burst disc allowing excess helium to be vented. In the event the poppet valve fails to reseat, the SOV is closed by the crew.

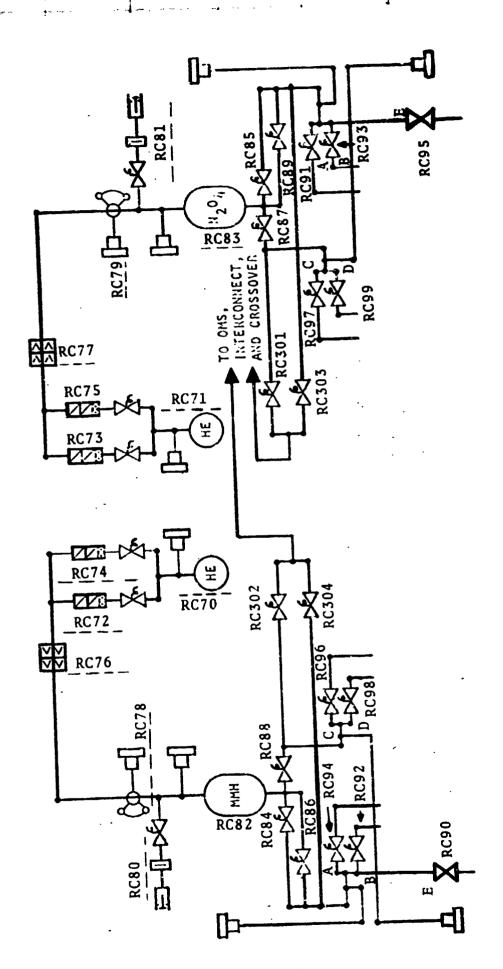
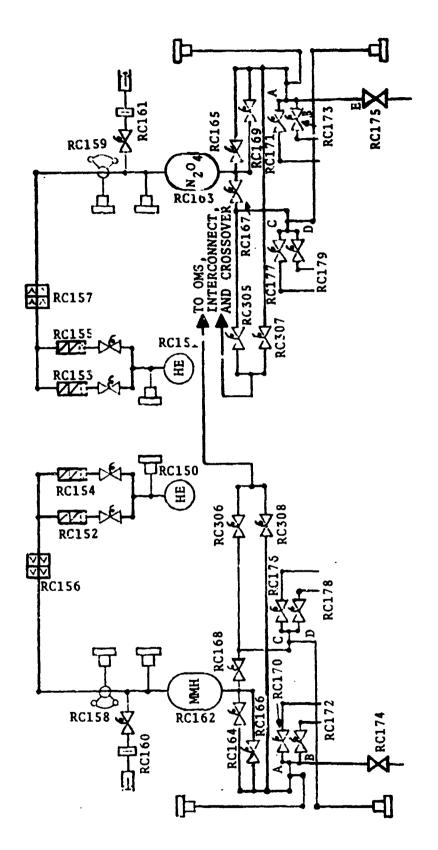


Figure 7. - Left aft RCS functional paths.

TO MANIFOLD ISOLATION VALVES

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Figure 8. - Left aft RCS functional path.



Pigure 9. - Right aft RCS functional paths.

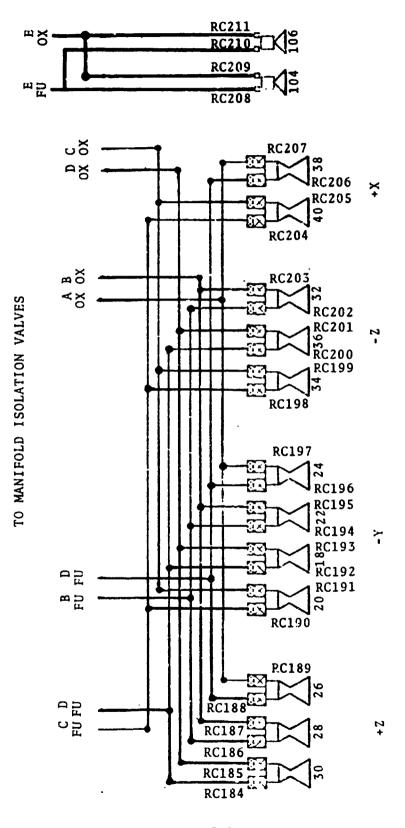


Figure 10. - Right aft RCS manifold functional paths.

RC82 and RC83 are propellant holding tanks. Each tank has a volume of approximately 14 cubic feet.

RC84 through RC89 are tank isolation valves used to isolate propellant flow from the propellant tanks to the thruster manifolds.

RC90 through RC99 are manifold isolation valves used to control the flow of propellant to three primary jets or two vernier jets. In the event of a failed-on thruster or a leak, the fuel and oxidizer manifold isolation valves associated with the failure are closed.

RC104 through RC131 are engine inlet valves for fuel and oxidizer. Each engine has a dedicated jet driver which opens and closes the fuel and oxidizer inlet valves on command.

# 5.3 Functional Path Description of Right Aft RCS

The right aft RCS has components identical to those in the left aft RCS. The functional path description is, therefore, the same as the left aft RCS except for the functional path numbering

## 5.4 Operating Functional Paths

The functional paths of the aft RCS are combined into operating functional paths for fault detection and annunciation. The operating functional paths are identified as ORCXXX. A total of 14 fuel and 14 oxidizer operating functional paths exist in each aft RCS.

5.4.1 Fuel operating functional paths - aft left RCS.
All 14 functional paths for fuel are identical from the helium source to the tank isolation valves. The common fuel path is identified as:

ORC100 = RC70 (RC72 + RC74) (RC76) (RC78) (RC82)

In addition, eight engines have a common fuel path through parallel tank isolation valves and the remaining six engines have a common path through the remaining tank isolation valve. The fuel paths are identified as:

ORC101 = (ORC100) (RC84 + RC86)

ORC102 = (ORC100) (RC88)

Past the tank isolation valves the functional paths branch to the manifolds as follows:

ORC103 = (ORC101) (RC94) Manifold A

ORC104 = (ORC101) (RC92) Manifold B

ORC105 = ORC101 (RC90) Manifold E

ORC106 = ORC102 (RC96) Manifold C

ORC107 = ORC102 (RC98) Manifold D

The complete fuel flow functional paths for the engines are given below:

ORC108 = (ORC103) (RC106) Engine 25

ORC109 = (ORC103) (RC114) Engine 23

ORC110 = (ORC103) (RC122) Engine 31

ORC111 = (ORC104) (RC110) Engine 21

ORC112 = (ORC104) (RC118) Engine 33

ORC113 = (ORC104) (RC124)Engine 37 ORC114 = (ORC105) (RC128)Engine 103 ORC115 = (ORC105) (RC130)Engine 105 ORC116 = (ORC106) (RC112)Engine 19 ORC117 = (ORC106) (RC104)Engine 27 ORC118 = (ORC106) (RC120)Engine 35 ORC119 = (ORC107) (RC108)Engine 29 ORC120 = (ORC107) (RC116)Engine 17 ORC121 = (ORC107) (RC126)Engine 39

5.4.2 Oxidizer operating functional paths - aft left RCS. The oxidizer operating functional paths are similar to the fuel operating functional paths and are compiled as follows.

The common path to the tank isolation valve is:

ORC122 = (RC71) (RC73 + RC75) (RC77) (RC79 (RC83)

The common oxidizer paths through the tank isolation paths are:

ORC123 = (ORC122) (RC85 + RC89)

ORC124 = (ORC122) (RC87)

The common oxidizer paths to the oxidizer manifolds are:

ORC125 = (ORC123) (RC91) Manifold A

ORC126 = (ORC123) (RC93) Manifold B

ORC127 = (ORC123) (RC95) Manifold E

ORC128 = (ORC124) (RC97) Manifold C

ORC129 = (ORC124) (RC95) Manifold D

The oxicizer operating functional flow paths to the engines are defined as follows:

ORC130	=	(ORC125)	(RC107)	Engine	25
ORC131	=	(ORC125)	(RC115)	Engine	23
ORC132	=	(ORC125)	(RC123)	Engine	31
ORC133	=	(ORC126)	(RC111)	Engine	21
ORC134	=	(ORC126)	(RC119)	Engine	33
ORC135	=	(ORC126)	(RC125)	Engine	37
ORC136	=	(ORC127)	(RC129)	Engine	103
ORC137	=	(ORC127)	(RC131)	Engine	105
ORC138	=	(ORC128)	(RC113)	Engine	19
ORC139	=	(ORC128)	(RC105)	Engine	27
ORC140	=	(ORC128)	(RC121)	Engine	35
ORC141	=	(ORC129)	(RC109)	Engine	29
ORC142	=	(ORC129)	(RC117)	Engine	17
ORC143	=	(ORC129)	(RC127)	Engine	39

5.4.3 Firel operating functional paths - aft right RCS. The operating functional fuel path from the helium source to the propellant tank SOV's is common to all 14 engines, and is identified as:

ORC200 = (RC150) (RC152 + RC154) (RC156) (RC158) (RC162)

The operating functional fuel flow path divides into two paths at the tank SOV's. They are defined as follows:

ORC201 = (ORC200) (RC164 + RC166)

ORC202 = (ORC200) (RC168)

The five operating functional fuel flow paths to the fuel manifolds are defined by:

ORC203 =	(ORC201)	(RC170)	Manifold	A
ORC204 =	(ORC201)	(RC172)	Manifold	В
ORC205 =	(ORC201)	(RC174)	Manifold	E
ORC206 =	(ORC202)	(RC176)	Manifold	С
ORC207 =	(ORC202)	(RC178)	Manifold	D

The complete operating functional fuel flow paths for the engines are given below:

ORC263	=	(ORC203)	(RC188)	Engine	26
		(onozoo)	(NOTOO)	Bilgine	20
ORC209	=	(ORC207)	(RC196)	Engine	24
ORC210	=	(ORC293)	(RC206)	Engine	38
CRC211	=	(ORC204)	(RC186)	ngine	28
ORC212	=	(ORC204)	(20194)	Engine	22
ORC213	=	(ORC204)	(RC202)	Engine	32
ORC214	=	(ORC205)	(RC208)	Engine	104
ORC215	=	(ORC205)	(RC210)	Engine	106
ORC216	=	(ORC206)	(RC190)	Engine	20
ORC217	=	(ORC206)	(RC189)	Engine	34
OPC218	=	(ORC206)	(RC204)	Engine	40
ORC219	=	(ORC207)	(RC184)	Engine	30
ORC220	=	(ORC207)	(RC192)	Engine	18
ORC221	=	(ORC207)	(RC200)	Engine	36

5.4.4 Oxidizer operating functional paths - aft right RCS. The oxidizer operating functional flow path from the helium source to tank SOV's is common to all engines and is defined as:

ORC222 = (RC151) (RC153 + RC155) (RC157) (RC159) (RC163)

The oxidizer operating functional flow paths through the tank SOV's are defined as:

ORC223 = (ORC222) (RC165 + RC169)

ORC224 = (ORC222) (RC167)

The oxidizer operating functional flow paths to the oxidizer manifolds are:

ORC225 = (ORC223) (RC171) Manifold A

ORC226 = (ORC223) (RC173) Manifold B

ORC227 = (ORC223) (RC175) Manifold E

ORC228 = (ORC224) (RC177) Manifold C

ORC229 = (ORC224) (RC179) Manifold D

The complete oxidizer operating functional flow paths for the engines are given below:

ORC230 = (ORC225) (RC189) Engine 26

ORC231 = (ORC225) (RC197) Engine 24

ORC232 = (ORC225) (RC207) Engine 38

ORC233 = (ORC226) (RC203) Engine 32

ORC234 = (ORC226) (RC195) Engine 22

ORC235 = (ORC226) (RC187) Engine 28

ORC236 = (ORC227) (RC209) Engine 104

ORC237	==	(ORC227)	(RC211)	Engine	106
ORC238	=	(ORC228)	(RC205)	Engine	40
ORC239	=	(ORC228)	(RC199)	Engine	34
ORC240	=	(ORC228)	(RC191)	Engine	20
ORC241	=	(ORC229)	(RC185)	Engine	30
ORC242	=	(ORC229)	(RC193)	Engine	18
ORC243	=	(ORC229)	(RC201)	Engine	36

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# 6.0 MEASUREMENT REQUIREMENTS FOR FAULT DETECTION AND ANNUNCIATION — AFT RCS

### 6.1 FDA Measurements

Tables 2 and 3 list the primary, correlation, and preconditioning measurements required for fault detection and annunciation for the right and left aft RCS. The tables identify 72 new measurements not included in the Master Measurements List, dated November 16, 1973. Measurement justification is also included in tables 2 and 3. Figures 11 through 14 show the approximate location of the aft RCS measurements.

- 6.2 Description of Parameters to be Monitored
- 6.2.1 Helium source pressure. Helium source pressure is used for propellant gauging and is the best overall indicator of system integrity. In the event the source pressure measurement fails, the system status and propellant remaining cannot be determined; therefore, redundant source pressure measurements should be added to the four helium tanks.
- 6.2.2 <u>Propellant pressures</u>. Helium SOV positions provide a precondition check to determine if the system is static or dynamic. Regulator output is required to isolate leaks and tailed components such as regulators, helium SOV's, and vent valves.

Tank outlet pressure provides a correlation check for regulator output pressure.

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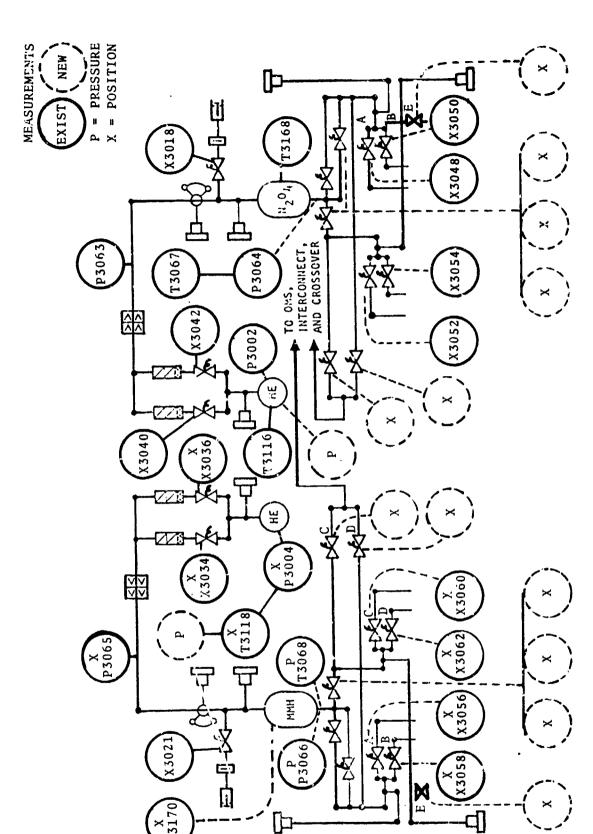


Figure 11. - Left aft RCS measurements for FDA.

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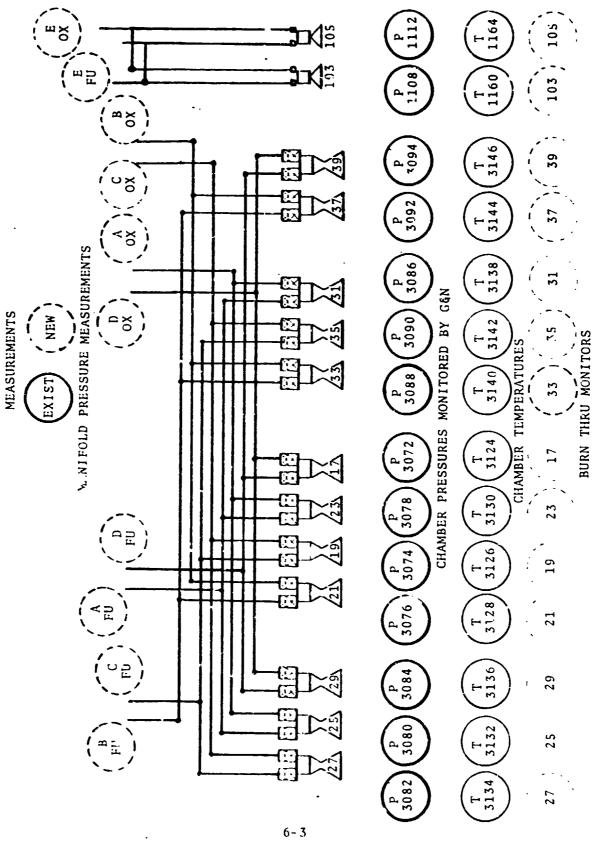


Figure 12. - Left aft RCS manifold measurements for FDA.

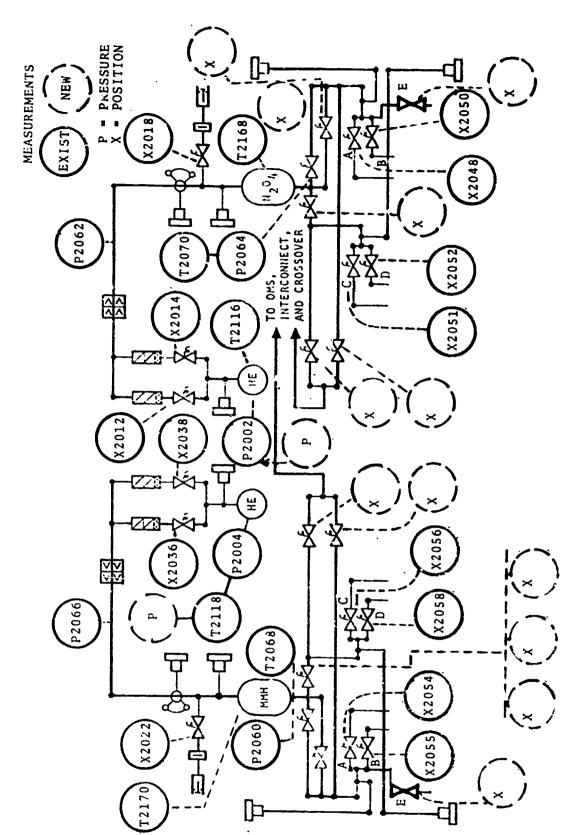


Figure 13. - Right aft RCS measurements for FDA.

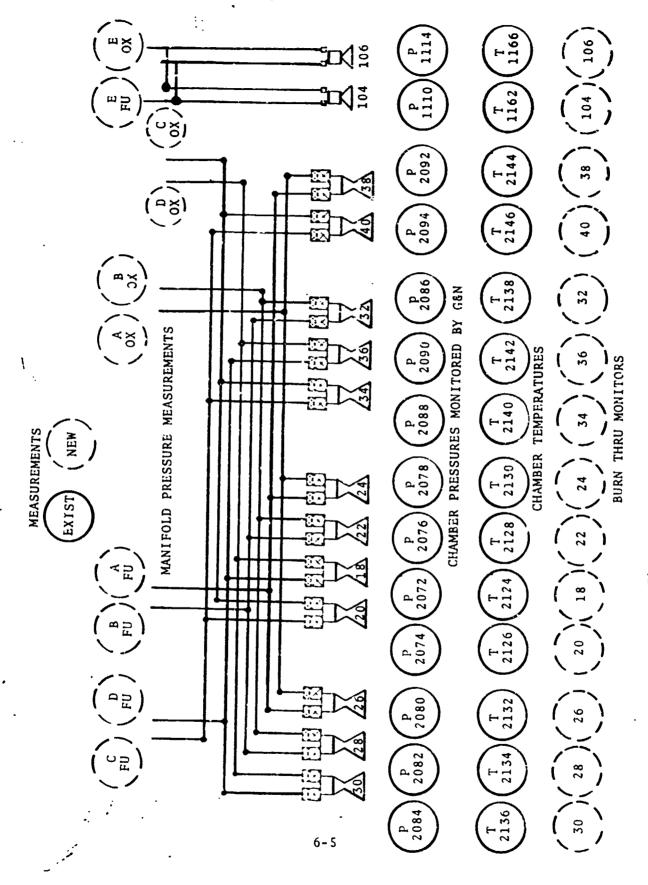


Figure 14. - Right aft RCS measurements.

6.2.3 <u>Manifold pressures</u>. Tank outlet SOV's, manifold isolation valves, and RCS crossfeed valve positions provide precondition checks for manifold pressure checks.

Manifold pressure transducers should be added to provide rapid leak isolation capability and engine inlet pressure monitoring during crossfeed operation. Heat soak back monitoring for isolated manifolds would also be provided by these transducers.

6.2.4 Thruster temperature. Thruster temperature transducers should be monitored for overtemperature during burns and for leak indications during quiescent periods.

In addition, the engine procurement specification provides for burn through monitors on each engine. It is anticipated that they will be monitored by PMS.

### 6.3 Leak Detection Methods

6.3.1 Quantity remaining. Premission helium profiles are not adequate for helium monitoring. Leaks can be detected by correlating helium source pressure with the quantity of propellant remaining. Since quantity remaining is gauged by helium pressure, volume, and temperature, quantity measurements become inaccurate when a leak is introduced into the system. A thruster-on time multiplied by flow rate calculation should be correlated with quantity remaining. Care must be exercised to charge propellant to the proper tanks during crossfeed operation.

6.3.2 <u>Delta pressure</u>. The helium source pressure delta for fuel and oxidizer should be nearly constant, since equal volumes of fuel and oxidizer are being consumed. A change in the delta pressure is indicative of a leak.

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA

<b>*</b>						l
S t t t t t s		Z		Z		
Justification	System status propellant gauging leak monitoring	ıng		Status and gauging lost if P2002A fails	Position defines type of monitoring static or dynamic	* New Measurement Required
Operating functional path	RC150 ORC200	RC150 ORC200	RC151 ORC222	RC151 ORC222	RC153 ORC222	w Measurem
Hard limit Correlation					NA	**N = Ne
	Propellant remaining dependent	Propellant remaining dependent	Propellant remaining dependent	Propellant remaining dependent	NA NA	
limit low					NA	
Soft					NA	
*⊃ v ə	ρ.	Ω	<u>n</u>	<u>a,</u>		5
Measurement	V42P2004A RCS R-aft He fuel tank pressure	RCS R-aft He fuel tank pressure #2	V42P2002A RCS R-aft He oxid tank pressure	RCS R-aft He oxid tank pressure	V42X2012E RCS R-aft He OX rgltr Isln valve 1	*P = Primary

C = Correlation

X = Precondition

TABLE 2. -- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

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8. tr g tr 2 a	ļ			<u> </u>		
Justification	Position defines type of monitoring static or dynamic	Safety insures vent line open	Safety insures vent line open	Position defines type of monitoring static or dynamic	Position defines type of monitoring static or dynamic	Isolated manifold monitor
Operating functional path	RC155 ORC222	RC161 ORC222	RC160 ORC200	RC152 ORC200	RC154 ORC200	RC171 ORC225
Correlation measurement	NA	NA	NA	NA	NA	NA
	NA	NA	NA	NA	NA	NA
Hard High	NA	NA	NA	NA	NA	NA
Soft limit Hard limit High low High low	NA	NA	NA	NA	NA	NA
Soft	NA	NA	NA	NA	NA	NA
*⊃ v o	×	×	×	×	×	
sur	V42X2014E RCS R-aft He OX rgltr valve 2	V42X2018E RCS R-aft He OX RLF	V42X2022E RCS R-aft He fu RLF valve	V42X2036E RCS R-aft He fuel rgltr Isln valve l	V42X2038E RCS R-aft He fuel rgltr Isln valve 2	V42X2048E RCS R-aft oxdzr thruste Isln valve A

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

N t t t t t t	1		1		
Justification	Isolated manifold monitor	Isolated marifold monitor	Isolated manifold monitor	Isolated manifold monitor	Isolated manifold monitor
Operating functional path	RC173 ORC226	RC177 ORC228	RC179 ORC229	RC170 ORC201	RC172 ORC204
ft limit Hard limit Correlation gh low High low measurement	NA	NA	NA	NA	NA
limit low	NA	NA	NA	NA	NA
Hard High	NA	NA	NA	NA	NA
limit low	NA	NA	NA	NA	NA
Soft	NA	NA	NA	NA	NA
*⊃ s e	Ъ	Ъ	д	Ъ	P
Measurement	V42X2050E RCS R-aft oxdzr thruster Isln valve B	V42X2051E RCS R-aft oxdzr thruster Isln valve C	V42X2052E RCS R-aft oxdzr thruster Isln valve D	V42X2054E RCS R-aft fu thrus.er isol valve A	V42X2055E RCS R-aft fu thruster isol valve B

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

C t a t z	W	Τ			Ţ	
Justification	Isolated manifold monitor	Isolated manifold monitor	Correlation CK for RGLTR pressure	Tank over- pressure monitor leak detection	Tank over- pressure monitor leak detection	Correlation for P2062A
Operating functional path	RC176 ORC205	RC178 ORC207	ORC200	ORC200	ORC222	ORC222
oft limit Hard limit Correlation igh low High low measurement	NA	NA	NA	P2060A	+1. P2064A	NA
limit low	NA	NA	TBD	270 psia	270 psia	TBD
Hard High	NA	NA	ТВD	300 psia	300 psia	TBD
limit low	NA	NA	TBD	TBD	ТВD	TBD
S H	A A	NA	ТВD	TBD	TBD	TBD
e s C*	C	D P	D C	P	Ъ	C
Measurement	E ter ve	er	V42P2060A RCS R-aft fuel prplt manf press	6 5	V42P2062A RCS R-aft oxdzr rgltr outlet press	742P2064A RCS R-aft oxd:r prplt nanf press

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

a t S	s u t						
	Justification	Heat and cold soak	Heat and cold soak	Heat and cold soak	Heat and cold soak	Temp and leak monitor	Temp and leak monitor
Operating	tunctional path	ORC200	ORC222	RC151	RC150	ORC220 ORC242	ORC216 ORC240
Correlation	measurement	P2170A	P2168A	NA	NA	NA	NA
limit	low	TBD	TBD	TBD	TBD	TBD	TBD
Hard	High	TBD	ТВД	TBD	ТВД	ТВD	Твр
ft limit	low	TBD	TBD	ТВD	TBD	TBD	ТВD
So	High	TBD	TBD	TBD	ГВD	TBD	Твр
*>	s	Ъ	Ь	Ъ	Ъ	ď	Ь
M. San	Measurement	V42T2068A RCS R-aft fuel mani- fold temp	V42T2070A RCS R-aft oxdzr mani- fold temp	V42T2116A RCS R-aft He oxdzr tk temp	V42T2118A RCS R-aft He fuel tank temp	V42T2124A RCS R-aft thruster injn temp No 18	V42T2126A RCS R-aft thruster injn temp No 20

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

νταταν						
justification	Temp and lesk monitor	Temp and leak monitor				
Operating functional path	ORC234 ORC212	ORC231 ORC209	CRC208 ORC230	ORC211 ORC235	ORC219 ORC241	ORC213 ORC233
Correlation measurement	NA	NA	NA	NA	NA	NA
Hard limit High low	ТВD	ТВD	TBD	ТВD	ТВD	TBD
High	TBD	TRD	ТВD	TBD	TBD	TBD
ft limit gh low	TBD	TBD	ТВD	ТВD	TBD	TBD
So Hi	ТВD	TBD	TBD	ТВD	TBD	TBD
Measurement s	V42T2128A RCS R-aft thruster injr temp No 22	V42T2130A RCS R-aft thruster injr temp No 24	V42T2132A RCS R-aft thruster injr temp No 26	V42T2134A RCS R-aft thruster injr temp No 28	V42T2136A RCS R-aft thruster injr temp No 30	742T2138A RCS R-aft thruster injr temp No 32

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

t S	s t t		1				
	Justification	Temp and leak monitor	Temp and leak monitor	Temp and leak monitor	Temp and leak monitor	Correlation for T2070A	Correlation for T2068A
Operating	functional path	ORC217 ORC239	ORC221 ORC243	ORC211 ORC232	ORC218 ORC238	ORC1 <b>6</b> 3	ORC162
limit Correlation	measurement	NA	NA	NA	NA	NA	NA
limit	low	ТВD	ТВD	TBD	TBD	TBD	ТВD
Hard	High	TBD	TBD	TBD	TBD	TBD	ТВD
limit	MOL	ТВD	TBD	ТВD	TBD	NA	NA
Soft	High	TBD	TBD	ТВD	ТВD	NA	NA
*=		<u> </u>		- <u> </u>		C	<u> </u>
	Measurement	V42T2140A RCS R-aft thruster injr temp No 34	V42T2142A RCS R-aft thruster injr temp No 36	V42T2144A RCS R-aft thruster injr temp No 38	V42T2146A RCS R-aft thruster injr temp No 40	V42T2168A RCS R-aft oxdzr tank shell temp	V42T2170A RCS R-aft fuel tank shell temp

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

S + B +	) J V	z	Z	Z	Z	z	Z	Z	Z
Justification		Leak isolation	Leak isolation	Leak isolation	Leak isolation	Leak isolation	Leak isolation	Leak isolation	Leak isolation
Operating functional	path	ORC203	ORC204	ORC206	ORC207	CRC205	ORC225	ORC226	ORC228
Correlation	measurement	NA	NA	NA	NA	NA	NA	NA	NA
Hard limit	low	TBD	ТВД	TBD	TBD	TBD	TBD	TBD	TBD
	High	TBD	TBD	ТВD	ТВD	TBD	ТВD	TBD	TBD
limit	1ок	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD
Soft	High	TBD	TBD	TBD	TBD	TBD	TBD	TBD	TBD
<b>*</b> ⊃ ′	ဂ်ပ	#	-6	D.	<del>D</del>	<del>-6</del>	Ъ	<del>a</del> i	<u>-</u>
Measurement		RCS R-aft fuel manifoldF A	. ~	RCS R-aft fuel manifoldP C	RCS R-aft fuel manifoldP D	RCS R-aft fuel manifoldP E	RCS R-aft ox manifold A	RCS R-aft ox manifold B	RCS R-aft ox manifold C

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

s t s	4 z s	z	z	Z	z	,2,	z	2.	Z
	Justilication	Leak isolation	Leak isolation	Safety	Safety	Safety	Safety	Safety	Safety
Operating	iunctional path	ORC229	CRC227	ORC220 ORC242	ORC216 ORC240	ORC234 ORC212	ORC231 URC209	ORC208 ORC230	0RC211 0RC235
Correlation	measurement	NA	NA						
Hard limit	10w	TBD	TBD	NA	NA	NA	NA	NA	NA
Hard	High	TBD	ТВD	NA	NA	NA	NA	NA	NA
limit	10w	TBD	TBD	NA	NA	NA	NA	NA	NA
Soft	High	TBD	TBD	NA	NA	NA	NA	NA	NA AN
*⊃	s e	נא	<u> </u>	<u>-</u>	<u> </u>	<u> </u>	<u>- 61</u>	<u>P</u>	<u></u>
N. C.		RCS R-aft ox manifold D	RCS R-aft ox manifold E	RCS R-aft thruster burnP thru No 18	RCS R-aft thruster burnP thru No 20	RCS R-aft thruster burnP thr No 22	RUS R-aft thruster burnP thru No 24	RCS R-aft thruster burnP thru No 26	RCS R-aft thruster burn thru No 28

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA -- Continued

N t a	なななる	Z	z	z	z	X	z	z	Z
	Justification	Safety	Safety	Safety	Safety	Safety	Safety	Safety	Safety
Operating	functional path	ORC219 ORC241	ORC213 ORC233	ORCZI7 ORCZ33	ORC221 ORC243	ORC211 ORC232	ORCZ18 ORC238	ORC736 ORC214	ORC237 ORC215
ft limit Hard limit Correlation	measurement	N.A.	NA	NA	VN	AN	NA	NA	NA
limit	10.4								
Hard	High	NA	NA	NA	NA	NA	N <	NA	NA
limit	low	NA	NA	NA	NA	NA	NA	NA	NA
Soft	High	NA	NA	NA	NA	NA	NA	NA	NA
*	e s C	а	Ч	<u>a</u>	=	- 63	rnP	2	2
	Measurement	RCS k-aft thruster burnP thru No 30	RCS P-aft thruster burnP thru No 32	RCS R-aft thruster burnP thru No 34	RCS R-aft thruster burn thru No 36	RCS R-aft thruster burn thru No 38	] = _	RCS R-aft thruster burn thru No 104	RCS R-aft thruster burn thru No 106

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Continued

	*=	Soft	t limit		Hard limit	Correlation	Operating		W + W
Measurement	രാ	High	low	High	low	measurement	tunctional path	Justification	<b>3</b> 2 4
PCS R-aft E fu manifold Isln valve position	а	NA	NA	Ϋ́	NA	NA	RC174 ORC205	Failed manifold monitor	z
RCS R-aft E OX manıfold Isln valve position	D,	Z A	\	VN	ΝΑ	NA	RC175 ORC227	Failed manifold monitor	z
RCS R-aft vernier 104 temp	Ь	TBD	TBD	ТВD	TBD	NA	ORC236 ORC214	Over temperature and leak monitor	Z
RCS R-aft vernier 106 temp	Ь	TBD	TBD	TBD	TBD	NA	ORC237 ORC215	Over temperature and leak monitor	z
RCS R-aft fu tank SOV 1	<b>;</b> <	NA	NA	NA	NA	NA	ORC202	Configuration	Z
RCS R-aft fu tank SOV 2	X	NA	NA	NA	NA	NA	ORC201	Configuration	z
RCS R-aft fu tank SOV 3	×	NA	NA	N.A.	NA	NA	ORC201	Configuration	z

TABLE 2.- RIGHT AFT RCS MEASUREMENTS FOR FDA - Concluded

Soft limit Hard limit Correlation Operating	limit Hard limit Correlation Opera	Hard limit Correlation Opera	limit Correlation Opera	Correlation Opera	Opera	ıting		t S
						functional	Justification	
High low High low measurement	1cw	1cw	1cw	measureme	nt	path		
NA NA NA NA	NA	NA		NA		ORC224	ORC224 Configuration	
NA NA NA NA	NA NA	VN		NA		ORC223	ORC223 Configuration	Z
NA NA NA NA	NA NA	NA		NA		ORC223	ORC223 Configuration	Z

TABLE 3.- LEFT AFT RC3 MEASUREMENTS FOR FDA

*	<u> </u>		I		<b></b>	
S t Justification a u s	System status propellant gauging leak monitor	Status and gauging lost if P3002A N fails	Safety insures tank vent line open	Safety insures tank vent line open	Position defines type of monitoring static or dynamic	Position defines type of monitoring static or dynamic
Operating functional path	RC71 ORC122	RC71 ORC122	RC81	RC80	RC72 RC100	RC74 RC100
Correlation		P3002A	VN	۷V	NA	NA
Hard limit High low	Propellant remaining dependent	Propellant remaining dependent	NA NA	NA NA	NA NA	NA NA
limit H.	TBD re	TBD re	NA	NA	NA	NA
Soft	T.B.D	ТВЪ	N A	N A	NA	NA
#⊃ v ⊕	<u></u>	d,	×	×	ь 1	- × 2
Measurement	V42P3002A RCS L-aft He oxdzr tk press	RCS L-aft He oxdzr tk press	V42X3018E RCS L-aft He ox RLF Isln valve	V42X3021E RCS L-aft He fu RLF Isin valve	E H	V42X3036E RCS L-aft He fu RGLTR Isln valve 2

\*P = Primary

\*\*N = New Moasurement Required

C = Correlation

X = Precondition

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

0 F	るななる				Z		
	Justification	Position defines type of monitoring static or dynamic	Position defines type of monitoring static or dynamic	System status propellant gauging leak monitor	System status and propellant gauging N lost if P3004A fails	Isolated manifold monitor	Solated manifold monitor
Operating	functional path	RC73 ORC122	RC75 ORC122	RC70 RC100	RC70 RC100	RC91 ORC125	RC93 ORC126
Correlation	measurement	NA	NA		P3004A		
Soft limit Hard limit	n low	NA	NA	Propellant remaining dependent	Propellant remaining dependent	NA	
Har	High	N A	NA	Proj   rema	Prop remaindepo	NA	
limit	Jow	NA	NA	ТВО	ТВО	NA	NA
Soft	High	NA	NA	ТВD	TBD	NA	A N
*	D S O	×	×	Ъ	Q.	<u>م</u> ۲	D. 1.
	Measurement	V42X5U40E RCS L-aft He ox RGLTR Isln valve 1	V42X3U42E RCS L-aft He ox RGLTR Isin valve 2	V4ZP3UU4A RCS L-aft He fuel tk press	RCS L-aft He ruel tk press #2	V4ZX3U48E RCS L-aft oxdzr thruster Isln valve A	V4ZX3USUE RCS L-aft oxdzr thruster Isin valve B

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

ats	s t t	[					
Justification		Isolated manifold monitor	Isolated manifold monitor	Isolated manifold monitor	Isolated manifold monitor	Isolated manifold monitor	Isolated manifold monitor
Operating functional	path	RC97 ORC128	RC99 ORC129	RC94 ORC103	RC92. ORC104	RC96 ORC106	RC98 ORC107
Correlation	measurement	NA	NA	NA	NA	NA	NA
limit	low	NA	NA	NA	NA	NA	NA
Hard	High	NA	NA	NA	NA	NA	NA
ft limit	low	NA	NA	NA	NA	NA	NA
So	High	NA	N A	NA	NA	NA	NA
*>	s o	—e —	- e -	ď	ъ	Ч	Д
Measurement		V42X3052E RCS L-aft P oxdzr thruster Isln valve C	ם	V42X3056E RCS L-aft fu thruster Isln valve A	V42X3058E RCS L-aft fu thruster Isln valve B	V42X3060E RCS L-aft fu thruster Isln valve C	V42X3062E RCS L-aft fu thruster Isln valve D

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

8 C T 2 A A				Ţ		1
Justification	Tank overpress leak isolation	Correlation for P3063A	Tank overpress leak isolation	Correlation for P3065A	Heat and cold soak	Heat and cold soak
Operating functional path	RC73 RC75 RC122	RC73 RC75 ORC122	RC72 RC74 ORC100	RC72 RC74 ORC100	ORC122	ORC190
Correlation	P3064A	NA	P3066A	NA	T3116A	T3118A
Hard limit High low	270 psia	270 psia	270 psia	270 psia	TBD	TBD
1 1	300 psia	300 psia	300 psia	300 psia	TBD	TBD
limit low	ТВD	TBD	ТВр	ТВD	TBD	TBD
Soft High	TBD	ТВО	TBD	TBD	TBD	ТВД
*D % 0	<u>C4</u>	C	ρı	C	<u> </u>	Ъ
sur	V42P3063A RCS L-aft ox RGLTR outlet press	V42F3U04A RCS L-aft Ox PRPLT manf press	V42F3U65A RCS L-aft fuel RGLTR outlet press	V42P3066A RCS L-aft fuel PRPLT manf press	V4Z13067A RCS L-aft ox manf temp	V42T3068A RCS L-aft fuel manf temp

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

	*=	Soft	limit	Hard	limit	Correlation	Operating		t to
Measurement	o o	High	low	High	]. OW	measurement	tunctional path	Justification	s t t
.ft	υ	TBD	TBD	TBD	TBD	NA	RC71	Correlation for T3067A	<b> </b>
V42T3118A RCS L-aft He fuel tk temp	C	TBD	TBD	ТВД	TBD	NA	RC70	Correlation for T3068A	
V42T3124A RCS L-aft thruster injr temp No 17	Ы	TBD	ŢBD	TBD	TBD	NA	ORC142 ORC120	Temp and leak monitor	
V42T3126A RCS L-aft thruster injr temp No 19	Ω,	ТВD	TBD	TBD	ТВD	NA	ORC138 ORC116	Temp and leak monitor	
jr	Ċ.	TBD	TBD	TBD	ТВD	NA	ORC133 ORC111	Temp and leak monitor	<b></b>
V42T3130A RCS L-aft thruster injr temp No 23	C <sub>1</sub>	TBD	ТВD	ТВD	ТВД	NA	ORC131 ORC109	Temp and leak monitor	

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

a t S	s to th						
	Justification	Temp and leak monitor					
Operating	runctional path	ORC130 ORC108	ORC139 ORC117	ORC141 ORC119	ORC132 ORC110	ORC134 ORC112	ORC140 ORC118
limit Hard limit Correlation	measurement	NA	NA	NA	NA	NA	NA
limit	low	ТВЪ	ТВD	TBD	TBD	ТВД	ТВD
Hard	High	TBD	TBD	TBD	TBD	TBD	TBD
	low	ТВD	TBD	TBD	TBD	TBD	TBD
Soft	s e High	TBD	TBD	Тво	твр	твр	TBD
*>		jrP	jrP	jrP	jrP	jrP	jr
Mescuroment		V42T3132A RCS L-aft thruster injr temp No 25	V42T3134A RCS L-aft thruster injr temp No 27	V42T3136A RCS L-aft thruster injr temp No 29	V42T3138A RCS L-aft thruster injr temp No 31	V42T3140A RCS L-aft thruster injr temp No 33	V42T3142A RCS L-aft thruster injr temp No 35

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

ברפרט	S				Z	Z	Z	Z
Justification	Temp and leak monitor	Temp and leak monitor	Heat and cold soak	Heat and cold soak	Safety	Safety	Safety	Safety
Operating functional path	ORC135 ORC113	ORC143 ORC121	RC83	RC82	ORC142 ORC120	OR/138 ORC116	ORCI33 ORC111	ORC131 ORC109
Correlation	NA	NA	NA	NA	NA	NA	NA	NA
limit low	TBD	TBD	ТВД	TBD	NA	NA	NA	NA
Hard	TBD	TBD	TBD	TBD	NA	٧N	NA	NA
limit low	TBD	TBD	TBD	ŢBD	NA	NA	NA	NA
Soft High	TBD	TBD	TBD	TBD	NA	NA	NA	NA
<b>*</b> ⊃ ∨ •	<del></del>	<u> </u>	P	ద	ď	ρţ	Ъ	Ы
Measurement	V42T3144A RCS L-aft thruster injr temp No. 37	V42T3146A RCS L-aft thruster injr temp No 39	V42T3168A RCS L-aft oxid tank shell temp	V42T3170A KCS L-aft fuel tank shell temp	Burn thru thruster 17	Burn thru thruster 19	Burn thru thruster 21	Burn thru thruster 23

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

νταταν	Z	Z	Z	Z	Z	Z	Z	N	Z	Z
Justification	Safety	Safety								
Operating functional path	ORCI30 ORCI08	ORC139 ORC117	ORC141 ORC119	ORC132 ORC110	ORC134 ORC112	ORC140 ORC118	ORC135 ORC113	ORC143 ORC121	ORC136 ORC114	ORC137 ORC115
Correlation	NA	NA								
Hard limit High low	NA	NA								
Hard High	NA	NA								
limit low	NA	NA								
Soft	NA	NA								
*D v e	Ь	ď	Ъ	Ь	Д	ρι	Ы	വ	а	Ы
Measurement	Burn thru thruster 25	Burn thru thruster 27	Burn thru thruster 29	Burn thru thruster 31	Burn thru thruster 33	Burn thru thruster 35	Burn thru thruster 37	Burn thru thruster 39	Burn thru thruster 103	Burn thru thruster 105

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

R H B H S	s z	Z	z	z	Z	Z	Z	Z
Justification	Leak isolation	Leak isolation	Leak isolation	Leak isolation				
Operating functional path	ORC103	ORC104	ORC106	ORC107	ORC105	ORC125	ORC126	ORC128
Correlation	NA	NA	NA	NA	NA	NA	NA	NA
limit low	TBD	TBD	TBD	TBD	TBD	TBD	ТВD	TBD
Hard High	TBD	TBD	TBD	TBD	TBD	TBD	TBD	ТВD
limit low	TBD	ТВD	TBD	TBD	TBD	TBD	ТВD	ТВD
Soft	TBD	TBD	TBD	TBD	ТВD	TBD	TBD	TED
*⊃ s e	<u>A</u>	Ъ	Ь	P	7	P	P	Ь
Measurement	RCS L-aft fuel manifold A	RCS L-aft fuel manifold B	RCS L-aft fuel manifold C	RCS L-aft fuel manifold D	RCS L-aft fuel manifold E	RCS L-aft ox manifold A	RCS L-aft ox manifold B	RCS L-aft ox manifold C

TABLE 3.- LEFT AFT RCS MEASUREMENTS FOR FDA - Continued

o + a + a	2	Z		Z	Z	2	2
Justification	Leak isolation	Leak isolation	Failed marifold monitor	Failed manifold monitor	Over temperature and leak monitor	Over temperature and leak monitor	Configuration
Operating functional path	ORC129	ORC127	RC90 ORC105	RC95 ORC127	ORC136 ORC128	ORC137 ORC130	ORC101
Correlation	NA	NA	۸X	NA	NA	NA	NA
Hard limit	ТВD	TBD	NA	NA	TBD	TBD	NA
<u> </u>	ТВD	TBD	NA	NA	TBD	TBD	NA
limit low	ТВD	TBD	NA	NA	TBD	TBD	NA
Soft	TBD	TBD	NA	NA	P TBD	ТВD	NA
*⊃ s ⊕	ద	ద	ď	Ъ	24	<u> </u>	_×
Measurement		RCS L∵aft ox munifold E	<b>~</b> #	א היו	RCS L-aft vernier 103 temp	RCS L-aft vernier 105 +emp	RCS L-aft fu tank SOV 1

TABLE 5.- LEFT AFT RCS MEASUREMENTS FOF FDA - Concluded

	*:	Sof	limit	Hard	limit	t limit Hard limit Correlation	Operating		ه دد دی
Measurement	၁ လ မ	High	10w	High	low	measurement	functional path	Justification	4 th 22 th
RCS L-aft fu tank SOV 2	×	NA	NA	NA	I.A	NA	ORC102	Configuration	Z
RCS L-aft fu tank SOV 3	х	NA	NA	NA	VK	NA	ORC102	Configuration	Z
RCS L-aft ox tank SOV 1	х	NA	NA	NA	NA	NA	ORC124	Configuration	N
RCS L-aft ox tank SOV 2	X	NA	NA	NA	NA	NA	ORC123	Configuration	Z
RFS L-aft ox tank SOV 3	X	NA	NA	NA	NA	NA	ORC123	Configuration	Z

## 7.0 RCS CROSSFEED OPERATION

# 7.1 Configuration

Additional fuel and oxidizer functional flow paths to the RCS manifolds are available from each tank on the crossfeed line.

The crossfeed configuration is shown in figures 15 and 16.

# 7.2 Operational Guidelines

To avoid propellant transfer due to differential pressure, only one propellant tank at a time is connected to its respective crossfeed line. To insure equal manifold pressure, the fuel and oxidizer tank connected to their respective crossfeed line are from the same subsystem.

The left and right aft RCS may be operated simultaneously from the crossfeed lines.

# 7.3 Crossfeed Components

Two additional shut-off valves connect each crossfeed line to the aft left and right RCS. These valves are identified as RC301 through RC308 (see figs. 15 an. 16).

7 4 Propellant Operating Functional Paths for RCS Crossfeed

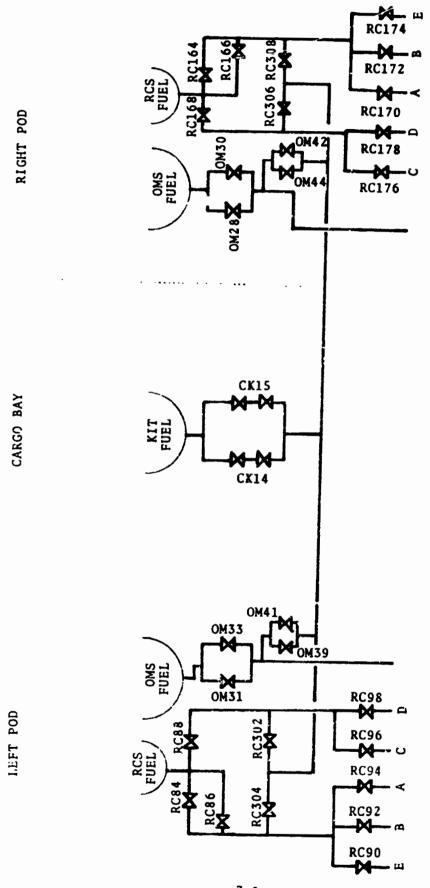


Figure 15. - Fuel crossfeed.

7-2

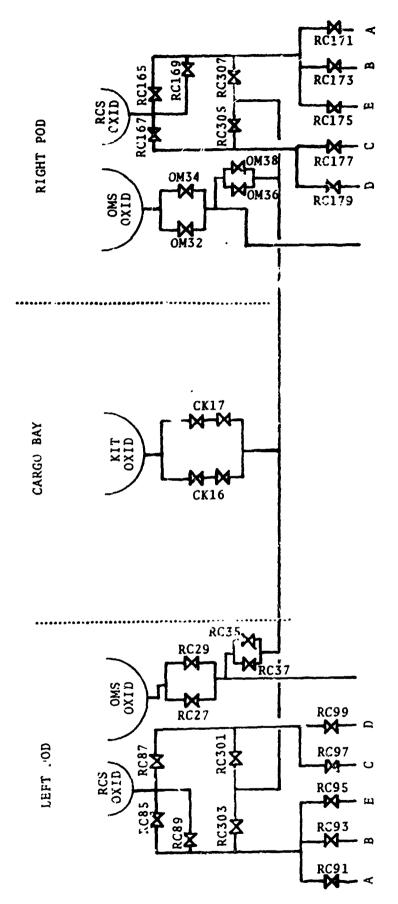


Figure 16. - Oxidizer crossfeed.

7-3

7.4.1 RCS fuel tanks to crossfeed line. The fuel operating functional paths from the tanks to the crossfeed lines are defined as follows:

Left aft RCS (ref. section 5.4.1)

ORC320 = (ORC100) [(RC84 + RC86) (RC304) +

(RC88) (RC302)]

Right aft RCS (ref. section 5.4.3)

ORC300 = (ORC200) [(RC164 + RC166) (RC308) + (RC168) (PC306)]

7.4.2 RCS oxidizer tanks to crossfeed lines. The oxidizer functional raths from the tanks to the crossfeed lines are defined as follows:

Left aft RCS (ref. section 5.4.2)

ORC321 = (ORC122) [(RC85 + RC89) (RC303) + (RC87) (RC30<sup>1</sup>)]

Right aft RCS (ref. section 5.4.4)

ORC301 = (ORC222) [(RC165 + RC169) (RC307) + (RC167) (RC305)]

- 7.4.3 Crossfeed from aft right RCS tanks to aft left RCS manifolds. The operating functional flow paths from the right aft RCS propellant tanks to the left aft RCS manifolds are given below (ref. sections 7.4.1 and 7.4.2):
  - A Fuel Manifold
     ORC302 = (ORC300) (RC304) (RC94)
  - B Fue Manifold
    ORC303 = (ORC300) (RC304) (RC92)

- E Fuel Manifold
  ORC304 = (ORC300) (RC304) (RC90)
- C Fuel Manifold
  ORC305 = (ORC300) (RC302) (RC96)
- D Fuel Manifold
  ORC306 = (ORC300) (RC302) (RC98)
- A Oxidizer Manifold
   ORC307 = (ORC301) (RC303) (RC91)
- B Oxidizer ManifoldORC308 = (ORC301) (RC303) (RC93)
- E Oxidizer ManifoldORC309 = (ORC301) (RC303) (RC95)
- C Oxidizer Manifold
  ORC310 = (ORC301) (RC301) (RC97)
- D Oxidizer Manifold
   ORC311 = (ORC301) (RC301) (RC99)
- 7.4.4 Crossfeed from aft left RCS tanks to aft right RCS manifolds. The operating functional flow paths from the left aft RCS propellant tanks to the right aft RCS manifolds are given below (ref. sections 7.4.1 and 7.4.2):
  - A Fuel Manifold
    ORC322 = (ORC320) (RC308) (RC170)
  - B Fuel Manifold
    ORC323 = (ORC320) (RC308) (RC172)
  - E Fuel Manifold
    ORC324 = (ORC320) (RC308) (RC174)

- C Fuel Manifold
  ORC325 = (ORC320) (RC306) (RC176)
- D Fuel Manifold
  ORC326 = (ORC320) (RC306) (RC178)
- A Oxidizer ManifoldORC327 = (ORC321) (ORC307) (RC171)
- B Oxidizer ManifoldORC328 = (ORC321) (ORC307) (RC173)
- E Oxidizer Manifold
  ORC329 = (ORC321) (ORC307) (RC175)
- C Oxidizer Manifold
  ORC330 = (ORC321) (ORC305) (RC177)
- D Oxidizer ManifoldORC331 = (ORC321) (ORC305) (RC179)

## 7.5 Measurements

No additional measurements are required for RCS cross-feed operation.

# 8.0 RCS, OMS INTERCONNECT OPERATION

# 8.1 Functional Paths for OMS/RCS Interconnect

The OMS functional paths used for RCS interconnect are shown in figure 17. The are identified as OMXX. Functional paths are combined into operating functional paths and identified as OOMXX.

# 9 : : unctional Path Analysis of OMS Propellant Path to Crossfeed Lines

GM1 and GM2 are helium source tanks. Each tank has a volume of 15.4 cubic feet. The tanks are pressurized to approximately 4000 psia prior to launch.

OM3 through OM6 are helium isolation shut-off valves in series with a primary and secondary helium regulator. Fank pressure is regulated to approximately 213 psig.

GM7 through OM10 are shut off valves to isolate oxidizer from the helium manifold during periods when tanks are not in use.

OM11, OM12, OM15, and OM16 are series parallel check valves to isolate propellant from the helium manifold.

OM13, OM14, OM17, and OM18 are manual shut-off valves used for ground servicing only.

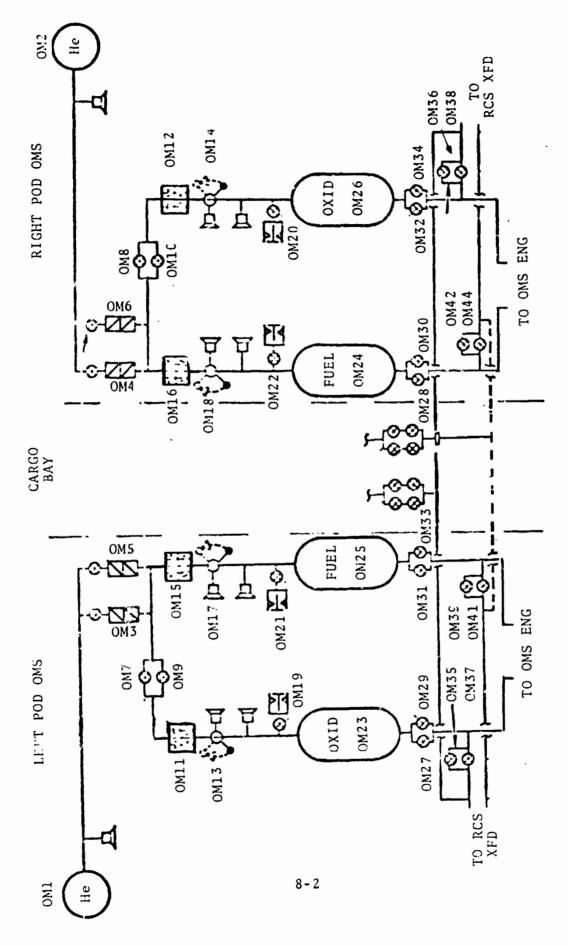


Figure 17. - Functional paths for OMS/RCS interconnect.

OM19 through OM22 are burst disc in series with poppet relief valves for relieving helium overboard, in the event a failure results in over pressurization of the tank.

OM23 through OM26 are propellant holding tanks. Each tank has a volume of approximately 89.5 cubic feet.

OM27 through OM34 are pairs of parallel redundant shutoff valves. Either valve in a pair can flow enough propellant to support an OMS engine burn.

OM35 through OM39 and OM41 through OM44 are pairs of parallel redundant shut-off valves. These valves connect the OMS manifolds to the crossfeed lines.

# 8.3 OMS Operating Functional Paths to the Crossfeed Lines

Operating functional paths for OMS propellant to the crossfeed lines are defined as follows (see fig. 17):

- Left pod OMS fuel to crossfeed line OOM1 = (OM1) (OM3 + OM5) (OM15) (OM17) (OM25) (OM31 + OM33) (OM39 + CM41)
- Left pod OMS oxidizer to crossfeed line OOM2 = (OM1) (OM3 + OM5) (OM7 + OM9) (OM11) (OM13) (OM23) (OM27 + OM29) (OM35 + OM37)
- Right pod OMS fuel to crossfeed line
  OOM3 = (OM2) (OM4 + OM6) (OM16) (OM18) (OM24)
  (OM28 + OM30) (OM42 + OM44)

- Right pod OMS oxidizer to crossfield line
   OOM4 = (OM2) (OM4 + OM6) (OM8 + OM10) (OM12)
   (OM14) (OM26) (OM32 + OM34) (OM36 + OM38)
- 8.4 Operating Functional Paths for Interconnect Left OMS to Left RCS Manifelds

The operating functional paths for supplying propellant from the left pod OMS tanks to the left pod RCS manifolds are defined as follows (ref. section 8.3):

- Left RCS fuel manifold A
   ORC340 = (OOM1) (RC304) (RC94)
- Left RCS fuel manifold B
  ORC342 = (OOM1) (RC304) (RC92)
- Left RCS fuel manifold E ORC344 = (OOM1) (RC304) (RC90)
- Left RCS fuel manifold C ORC346 = (00M1) (RC302) (RC96)
- Left RCS fuel manifold D ORC348 = (OOM1) (RC302) (RC98)
- Left RCS oxidizer manifold A
   ORC341 = (OOM2) (RC303) (RC91)
- Left RCS oxidizer manifold B
   ORC343 = (OOM2) (RC303) (RC93)
- Left RCS oxidizer manifold E
   CRC345 = (OOM2) (RC303) (RC95)
- Left RCS oxidizer manifold C
   ORC347 = (OOM2) (RC301) (RC97)

- Left RCS oxidizer manifold D
   ORC349 = (OOM2) (RC301) (RC99)
- 8.5 Operating Functional Paths for Interconnect
  Right OMS to Left RCS Manifolds

The operating functional paths for supplying propellant from the right pod OMS tanks to the left pod RCS manifold are defined as follows (ref. section 8.3):

- Left RCS fuel manifold A
   ORC350 = (OOM3) (RC304) (RC94)
- Left RCS fuel manifold B OP.C352 = (OOM3) (RC304) (RC92)
- Left RCS fuel manifold E
   ORC354 = (OOM3) (RC304) (RC20)
- Left RCS fuel manifold C
   ORC356 = (OOM3) (RC302) (RC96)
- Left RCS fuel manifold D ORC358 = (OOM3) (RC302) (RC98)
- Left RCS oxidizer manifold A
   ORC351 = (OOM4) (RC303) (RC91)
- Left RCS oxidizer manifold B ORC353 = (OOM4) (RC303) (RC93)
- Left RCS oxidizer manifold E ORC355 = (OMM4) (RC303) (RC95)
- Left RCS oxidizer manifold C ORC357 = (OMM4) (RC301) (RC97)

- Left RCS oxidizer manifold D ORC359 = (OMM4) (RC301) (RC99)
- 8.6 Operating Functional Paths for Interconnect
  Lert OMS to Right RCS Manifolds

The operating functional paths for supplying propellant from the left OMS pod to the right RCS manifolds are defined as follows (ref. section 8.3):

- Right RCS fuel manifold A
   ORC360 = (OOM1) (RC308) (RC170)
- Right RCS fuel manifold B
  ORC362 = (OOM1) (RC308) (RC172)
- Right RCS fuel manifold EORC364 = (OOM1) (RC308) (RC174)
- Right RCS fuel manifold C
   ORC366 = (OOM1) (RC306) (RC176)
- Right RCS fuel manifold D ORC368 = (OOM1) (RC306) (RC178)
- Right RCS oxidizer manifold A ORC361 = (OOM2) (RC307) (RC171)
- Right RCS oxidizer manifold B
   ORC363 = (OOM2) (RC307) (RC173)
- o Right RCS oxidizer manifold E ORC365 = (OOM2) (RC307) (RC175)
- Right RCS oxidizer manifold C
   ORC367 = (OOM2) (RC305) (RC177)

- Right RCS oxidizer manifold D
   ORC369 = (OOM2) (RC305) (RC179)
- 8.7 Operating Functional Paths for Interconnect Right OMS to Right RCS Manifolds

The operating functional paths for supplying propellant from the right OMS pod to the right RCS manifolds are defined as follows (ref. section 8.3).

- Right RCS fuel manifold 'ORC370 = (OOM3) (RC30%, (RC170)
- Right RCS fuel manifold B
  ORC372 = (OOM3) (RC308) (RC172)
- Right RCS fuel manifold E
   ORC374 = (OOM3) (RC308) (RC174)
- Right RCS fuel manifold C ORCC76 = (00M3) (RC306) (RC176)
- Right RCS fuel manifold D ORC378 = (OOM3) (RC306) (RC178)
- Right RCS oxidizer manifold A
   ORC371 = (OOM4) (RC307) (RC171)
- Right RCS oxidizer manifold B
   ORC373 = (OOM4) (RC307) (RC173)
- Right RCS oxidizer manifold E
   ORC375 = (OOM4) (RC307) (RC175)
- Right RCS oxidizer manifold C
   ORC377 = (OOM4) (RC305) (RC177)
- Right RCS oxidizer manifold D ORC379 = (OOM4) (RC305) (RC179)

## 8.8 Crossfeed Single Point Failure

During OMS burns when the OMS engines are being supplied propellant (from the cargo bay kit) through the crossfeed lines, the RCS crossfeed valves are a single point failure. If an RCS crossfeed valve fails open, the OMS engine will be supplied from the RCS tank, since it is at a higher pressure than the cargo bay kit. In addition to depleting the RCS propellant, the OMS inlet dela pressure limit will be exceeded.

A study is presently being conducted to determine if this problem can be resolved by changing the RCS and CMS ullage pressure.

### 8.9 Measurements

The measurements required for fault detection and annunciation for OMS/RCS interconnect operation are given in tables 4 and 5.

Six new measurements have been identified to be added to the Master Measurements List.

Four new measurements are required for monitoring valve position of new tank SOV's that were added to the system. In addition, redundant helium source pressure transducers should be added. System status is lost if helium source pressure cannot be determined.

TABLE 4. - LEFT OMS MEASUREMENTS FOR FDA DURING LEFT OMS/RCS

# INTERCONNECT

ŀ	N + E + 3 #			1		
	Justification	Verify prepellant flow path	Verify line condition	Insure flow path	Verify closed line	Insure flow path
	Operating functi : path	2M2.7 2OM2.7	00M2	OM3 OOM2	00W 2	OM35 OOM2
	* Soft limit Hard limit Correlation U S High low High low measurement					
	limit low	NA	TRU	NA	NA	N N
	Hard High	N A	TBD	Ϋ́N	VN	A A
	limit Hard	NA	ТВО	NA	NA	NA
	* Soft Substantial	Υ V	rBD	NA	A A	NA
	* D % 0	Δ.	×	Д	×	C.
	Measurement	V. XXIZISE UMS-L Eng OX Isin valve position	V43T1263A OMS-L Eng OX XFD line temp	V43X13, JE OMS-L Eng He OX Isin valve position	V43X1316E OMS-1. Eng OX dump valvo position	V43X1Z6SE OMS-L Eng OX XFD valve 1 position

\*P = Primary

\*\*N = New Measurement Required

C = Correlation
X = Precondition

TABLE 4. - LEFT OMS MEASUREMENTS FOR THA DURING LEFT OMS/RCS

# INTERCONNECT - Continued

v t t t z w	<u> </u>	<del> </del>	<u> </u>	<del>}</del>	<b>}</b>	<b></b>
Justification	Insure flow puth	Insure flow puth	Voriíy líne condition	System management	Leak monitor	System munagement
Operating functional path	OM39 OOM1	OM41 00M1	00M1	00M1	00M1	OM2 S 00M1
Soft limit Hard limit Correlation High low High low measurement						
limit Iow	NA	N N	TRO	Mission dependent	NA	TBD
Hard High	٧N	۷N	TBD	Mis	٧N	Твр
limit low	NA	NA	TBD		NA	TBD
Soft	N N	<b>V</b> ?:	X 7.18D		۷ ۷	P TBD
ಕ⊏ ೫ ೮	<u>۔</u>	ı.	>:	ď	Ъ	£.
Measurement	1065E L ing XFD	1068E L Eng XFD e 2	V43T1063A OMS-L F. ; fuel XFD line temp	NO70A L Eng tank tity	V43X1072fi OMS-L ling fucl tank low lovel	V43T1074A OMS-L Eng fuel tank temp

TABLE 4.- LEFT OMS MEASUREMENTS FOR FDA PURING LEFT OMS/RCS

INTERCONNECT - Continued

							T		i
Measurement	*⊃ v	Soft	limit	Hard	limit	ft limit Hard limit Correlation	Operating functional	Justification	N + B +
	ေ	High	1 ow	High	low	measuroment	path		3 ×
74301270A DMS-L Eng Dxid tank	d			Mis	Mission dependent		00M2	Consumables management leak detection	
V43X1116E OMS-L Eng X fuel dump	× c	A N	V V	N A	Ϋ́ N		00M1	Verify closed	1
272E Eng nk evel		TBD	ТВД	Твр	TBD		OOM2	System management	44
V43T1274A OMS-L Eng OX tank temp - lower	C,	ТВО	TBD	270	200		OM23 OOM2	Leak detection	
V43P1276A OMS-L Eng OX tank ullage pressure	ď	۷۷	NA	NA	NA		0M23 00M2	Insure path flow	

TABLE 4. - LEFT OMS MEASUREMENTS FOR FDA DURING LEFT OMS/RCS

INTERCONNECT - Continued

s t t a t s				1		
Justification	Leak monitor	System status leak detection	System management	Verify flow path	Verify flow path	Verify flow path
Operating functional path	0M2.5 00M1	OM1 OOM1 OOM2	OM1 OOM1 OOM2	OM3 OOM1 OOM2	OM7 00M2	0M9 00M2
Correlation						
limit	200	llant ning dent	ТВр	AN	٧×	NA
limit Hard limit low High low	270	Propellant remaining dependent	TBD	N A	NA	NA
limit low	TBD	ТВЪ	ТВД	VZ VZ	NA	NA
Soft High	TBD	ТВр	TBD	NA	NA	NA
*⊃ v e	£, };	ď	ď	٩ c	Сı	Сı
Measurement	V43P1076A OMS-L Eng fuel tank ullage pressu	1100A L Eng H sure	V43T1105A OMS-L Eng He tank temp	V43XIII0E OMS-L Eng He fuel isln valve positi	1114E L vap valv sitio	XIII -L va n val

TABLE 4.- LEFT OMS MEASUREMENTS FOR FDA DURING LEFT OMS/RCS

# INTERCONNECT - Concluded

N + & + 1 m		Z	z	z	
Justification	Verify flow path	Loss of PII00A results in loss of system status	Verify flow puth	Insure open line N	Insure open line
Operating functional path	OM37 OGM2	OM1 OOM1 OOM2	OM3 OOM1 OOM2	0M31 00M1	OM33 OOM1
Soft limit Hard limit Correlation s High low measurement					
limit low	NA	Propellant remaining dependent	NA	NA	NA
Hard High	NA	Prop reme	A N	A A	NA
Soft limit High low	NA	ТВД	NA	NA	NA
Soft High	νA	eP TBD	A A	N A	N A
e s C≯	Ъ	<u>a</u>	а	<u>d</u>	ط ڈا
Measurement	V43X1268E OMS-L Eng OX XFD valve 2 position	ssur	OMS-L Eng OX Isin valve No 2 position		V43X1015E OMS-L Eng fuel Isln valve positi

TABLE 5.- RIGHT OMS MEASUREMENTS FOR FDA DURING RIGHT OMS/

RCS INTERCONNECT

stats		<u> </u>			
Justification	Consumables management leak detection	Insure no propellant dep.etion	Systom management	Leak monitor	System management
Operating functional path	OM24 OOM3	00M3	OM24	OM24 0OM3	OM2
Soft limit Hard limit Correlation s e High low High low measurement					
limi† low	ion dent	NA	TBD	200	ΥBD
Hard limi: High low	Mission dependent	NA	TBD	270	TBD
limit low		NA	TBD	TBD	TBD
Soft U S High		NA	р Твр	P TBD	р твр
es C*	Ъ	P	c <sub>4</sub>	P	Ъ
Mr surement	V43Q2070A OMS-R Eng Euel tank quantity	V43X2072E OMS-R Eng fuel tank low level	V43T2074A OMS-R Eng fuel tank temp	V43P2070A OMS-R Eng fuel tank ullage pressu	V43T2105A OMS-R Eng He tank temp

\*P = Primary

\*\*N = New Measurement Required

C - Correlation

X = Precondition

TABLE 5.- RIGHT OMS MEASUREMENTS FOR FDA DURING RIGHT OMS/RCS INTERCONNECT - Continued

TABLE 5.- RIGHT OMS MEASUREMENTS FOR FDA DURING RIGHT OMS/

RCS INTERCONNECT - Continued

***	s 1eak	s leak agement	leak lagement
Justification Consumables	management leak detection Insure no propellant depletion	management leak detection Insure no propellant depletion System management	management lea detection Insure no propellant depletion System managem Leak detection
functional path	00M4	00M4 00M4 0M25	00M4 0M26 0M26 0M26
High low High low measurement  Mission			
High low Mission aependent	NA	NA	NA TBD
High Miss aepen	NA	NA TBD	NA TBD 270
low	NA	NA TBD	NA TBD
High	NA NA		NA TBD TBD
*D & G	Ωı		A A A
ent	13X2272E MS-R Eng K tank	43X2272E MS-R Eng X tank Tank WS-R Eng MS-R Eng X tank	V43X2272E OMS-R Eng OX tank Iow level V43T2.74A OMS-R Eng OX tan.k temp V43P2276A OMS-R Eng OX

TABLE 5.- RIGHT OMS MEASUREMENTS FOR FDA DURING RIGHT OMS/

RCS INTERCONNECT - Continued

N to a to a N				Z
Justification	Verify closed line	Verify closed line	Verify propellant flow path	Verify propellant flow path
Operating functional path	00M3	00M3	00M4	OOM4
Soft limit Hard limit Correlation  S High low High low measurement				
limit low	NA	NA	NA	NA
Hard limit High low	NA	NA	NA	NA
limit low	NA	NA	NA	NA
Soft limit s s High low	NA	NA	NA	NA
s G	X uo	×	P	J
Measurement		V43X2316E OMS-R Eng OX dump valve position	V43X2215E OMS-R Eng OX isln valve position	OMS-R Eng OX isln valve position

TABLE 5.- RIGHT OMS MEASUREMENTS FOR FDA DURING RIGHT OMS/
RCS INTERCONNECT - Continued

s t d t t a		Z			
Justification	Insure open line	Insure open line	Verify line condition	Insure flow path	Insure flow path
Operating functional path	00M3	00M3	00M3	00M3	00M3
Correlation measurement					
Soft limit Hard limit High low High low	NA	NA	ТВD	NA	NA
High	NA	NA	TBD	NA	NA
limi. low	NA	NA	TBD	NA	NA
Soft	NA	NA	ТВр	NA	NA
e v C*	P	Ъ	×	Ь	Ф
Measurement	V43X2015E OMS-R Eng fuel isln valve 1	OMS-R Eng fuel isln vaive 2	V43T2063A OMS-R Eng fuel XFD line temp	V43X2065E OMS-R Eng fuel XFD valve No 1 position	V43X2068E OMS-R Eng fuel XFD va've No 2 position

TABLE 5.- RIGHT OMS MEASUREMENTS FOR FDA DURING RIGHT OMS/

RCS INTERCONNECT - Concluded

<del></del>									2
Weasurement	*⊃	Soft	limit	Hard	limit	Soft limit Hard limit Correlation Operating U	Operating functional	Justification	t) 40 t
	e o	High	s e High low	High low	low	measurement	path		אבי
	×	TBD	TBD TBD	TBD	TBD		00M4	Verify line condition	<del></del>
perature	_								$\dashv$
OX No	ď	NA	NA	NA	NA NA		OM32 OOM4	Insure flow path	
V43X2268E OMS-R Eng OX XFD valve No 2 position	Ч	NA	NA	NA	NA		0M34 00M4	Insure flow path	

# 9.0 RCS INTERCONNECT TO CARGO BAY AUXILIARY PROPELLANT KIT

Additional propellant flow operating functional paths are available to the RCS manifolds from the cargo tay auxiliary propellant kits.

The functional paths of the auxiliary propellant from the cargo bay kit to the crossfeed lines are shown in figure 18. The functional paths are identified as CKXX and are combined into operating functional paths identified as OCKXX.

# 9.1 Functional Path Analysis of Auxiliary Propellant to Crossfeed Line

The cargo bay kits are added when more OMS delta velocity is required than can be supplied by the dedicated OMS tanks. Each kit consists of a fuel tank, an oxidizer tank, and a helium source bottle. One to three kits may be added to the cargo bay. The propellant tanks are connected in series, and the helium tanks are added in parallel.

CK1 consists of from one to three helium source bottles connected to a common manifold. Each bottle has a volume of 15.4 cubic feet.

CK3 is a shut-off valve allowing helium to be loaded from a ground source during servicing.

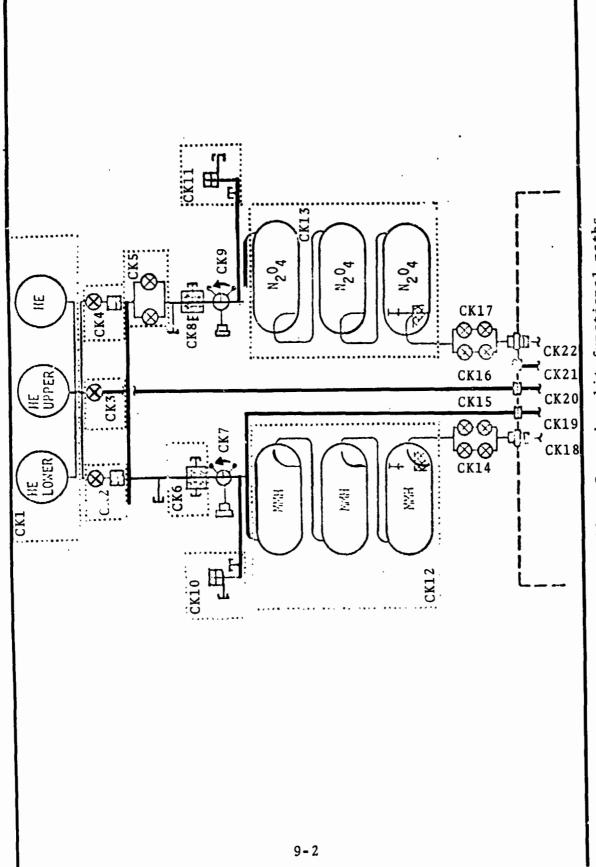


Figure 18. - Cargo bay kit functional paths.

CK2 and CK4 consist of helium isolation valves in series with a primary and secondary helium pressure regulator. The primary regulator regulates the output to 218 psig.

CK5 consists of two helium isolation valves in parallel used for positive isolation of  $N_2O_4$  from the nelium manifold. These valves remain closed when the cargo bay kits are not in use.

CK6 and CK8 are series parallel check valves which isolate propellants from the helium manifold.

CK7 and CK9 are manual shut-off valves used during ground servicing only.

CK10 and CK11 consist of a burst disc and poppet relief valve. In the event the tanks are subjected to over pressure, the burst disc ruptures and the excess helium vents overboard through the poppet relief valve.

CK12 and CK13 are propellant holding tanks. Each tank has a volume of approximately 89.5 cubic feet. Each kit contains a fuel and an oxidizer tank. A maximum of three kits may be installed in a vehicle.

CK14 through CK17 are series parallel shut-off valves which isolate the cargo bay kit propellants from the crossfeed lines.

CK18 through CK22 are bulkhead disconnects and feedthroughs from the cargo bay to the aft fuselage.

# 9.2 Cargo Bay Kit Operating Functional Paths to the Crossfeed Lines

Operating functional paths, for auxiliary propellant from the cargo bay kit to the crossfeed lines, are defined as follows (see fig. 18):

- Cargo bay auxiliary fuel to crossfeed line
   OCK1 = (CK1) (CK2 + CK4) (CK6) (CK7)
   (CK12) (CK14 + CK15) (CK18)
- Cargo bay auxiliary oxidizer to crossfeed line OCK2 = (CK1) (CK2 + CK4) (CK5) (CK8) (CK9) (CK13) (CK16 + CK17) (CK22)
- 9.3 Cargo Bay Kit Operating Functional Paths to Aft Left RCS Manifolds

The functional paths of the auxiliary propellant from the cargo bay kit to the left aft RCS manifolds are defined as follows (see figs. 11 and 12):

- Left aft RCS fuel manifold A
   OCK380 = (OCK1) (RC304) (RC94)
- Left aft RCS fuel manifold B
   OCK382 = (OCK1) (RC304) (RC92)
- Left aft RCS fuel manifold E
   OCK384 = (OCK1) (RC3C4) (RC90)
- Left aft RCS fuel manifold C
   OCK386 = (OCK1) (RC302) (RC96)
- Left aft RCS fuel manifold D
   OCK388 = (OCK1) (RC302) (RC96)

- Left aft RCS oxidizer manifold A
   OCK381 = (OCK2) (RC303) (RC91)
- Left aft RCS oxidizer manifold B
   OCK383 = (OCK2) (RC303) (RC93)
- Left aft RCS oxidizer manifold E
   OCK385 = (OCK2) (RC303) (RC95)
- Left aft RCS oxidizer manifold C
   OCK387 = (OCK2) (RC301) (RC97)
- Left aft RCS oxidizer manifold D
   OCK389 = (OCK2) (RC301) (RC99)

# 9.4 Cargo Bay Kit Operating Functional Paths to Aft Right RCS Manifolds

The functional paths of the auxiliary propellant from the cargo bay kit to the right aft RCS manifolds are defined as follows (see figs. 11 and 12):

- Right aft RCS fuel manifold A
   OCK390 = (OCK1) (RC308) (RC170)
- Right aft RCS fuel manifold B
   OCK392 = (OCK1) (RC308) (RC172)
- Right aft RCS fuel manifold E
   OCK394 = (OCK1) (RC308) (RC174)
- Right aft RCS fuel manifold C
   OCK396 = (OCK1) (RC306) (RC176)
- Right aft RCS fuel manifold D
   OCK398 = (OCK1) (RC306) (RC178)

- Right aft RCS oxidizer manifold A
   OCK391 = (OCK2) (RC307) (RC171)
- Right aft RCS oxidizer manifold B
   OCK393 = (OCK2) (RC307) (RC173)
- Right aft RCS oxidizer manifold E
   OCK395 = (OCK2) (RC307) (RC175)
- Right aft RCS oxidizer manifold C
   OCK397 = (OCK2) (RC305) (RC177)
- Right aft RCS oxidizer manifold D
   OCK399 = (OCK2) (RC305) (RC179)

#### 9.5 Measurements

The measurements required for RCS fault detection and annunciation are listed in table 6. Five new measurements (not in the Master Measurements List), dated November 16, 1973, are identified.

Since helium pressure provides the best overall system status as well as a means of propellant gauging, the measurement should be redundant.

Tank pressures are required for leak isolation and overpressure monitoring. At least one pressure transducer should be added to the fuel and oxidizer tanks.

Position indicators are required to indicate the position of the SOV's in functional paths CK14 through CK17. An indicator should be added to monitor the status of each path or, preferably, the status of each valve.

TABLE 6.- AUXILIARY PROPELLANT KIT MPASUKEMENTS REQUIRED FOR

RCS FDA

TA TA	<b>6</b> D 7	WI			_									
		-+			+					1		I	Z	
	Justification		System status	leak monitor	System status	lost if PO100A	faile	Crossfeed	configuration	Crossfeed	configuration	Overpressure	monitor leak	monitor
Operating	functional path	CKI	OCKI	OCK2	CKI	OCK1	OCK2	CK4	OCK2	CK2	OCK1		CX12	
Soft limit Hard limit Correlation	measurement					POIOOA								
limit	High low	Propellant	remaining	dependent	Propellant	remaining	dependent	NA		NA		2,40	007	
Hard		Prop	rema	debe	Frop	rema	deper	NA		NA		210	9	
limit	104							NA		NA		TRD		
	High							NA		NA		TBD		
*5			۵,	$oxed{\mathbb{I}}$		۵.		×	7	×	+	<u>۔</u>		1
A STATE OF THE STA		V43P0100A OMS He tank	pressure	aux.	UMS He tank	pressure aux No 2	V43X0310F	OMS-He OX Isln valve	pos aux	fuel	pos aux	ruel tank No 1	pressure	

\*P = Primary

C = Correlation

\*\*N = New Measurement Required

X - Precondition

TABLE 6.- AUXILIARY PROPELLANT KIT MEASUREMENTS REQUIRED FOR

RCS FDA - Continued

ν <del>ε 4 ε 4 ι</del>	Z		1	Z	
Justification	Overpressure monitor leak monitor	Crossfeed configuration	Crossfeed configuration	Crossfeed configuration	Crossfeed configuration
Operating functional path	CK13 OCK 2	CK5 CCK2	CKS OCK2	CK16 OCK2	CK17 0CK2
Correlation					
ft limit Hard limit gh lcw High low	260	NA	NA	NA	NA
Hard High	210	VN	NA	NA	NA
limit lcw	T 3D	NA	NA	NA	NA
Soft	TBD	NA	NA A	NA	NA
<b>*</b> ⊃ v o	4	×	×	×	×
Measurement	OX tank No 1 pressure	V43X0314E OMS vapor Isin valve Ng 1 pos - aux	V43X0315E OMS vapor Isln valve Nq 1 pos - aux	V43X0215E OMS OX Isln valve pos - aux	OMS oxidizer Isln valve pos - aux

TABLE 6.- AUXILIARY PROPELLANT KIT MEASUREMENTS REQUIRED FOR

RCS FDA - Continued

	Soft	oft limit	Hard limit	limit	Correlation	Operating		8 2 6
0	High	10w	High	low	measurement	functional path	Justification	1 7 3 8
V43X001SE OMS-fuel Isln valve pos - aux	NA	NA	NA	NA		CK14 OCK1	Crossfeed conf.guration	Z
OMS fuel Isln valve No 2 pos - aux	NA	NA	NA	NA		CK15 OCK1	Crossfeed configuration	Z
V43X0072E OMS fuel tank No 1 level low	NA	NA	NA	NA		OCK1	Insure no depiecion burns	
V43X02/2E OMS OX tank No 1 level low	NA	NA	NA	NA		OCK2	Insure no depletion burns	
ankX	TBD	TBD	TBD	BD		CK12 0CK1	System management	
V43T0075A OMS fuel tankx No 2 bulk temp - aux	TBD	ТВD	TBD	TBD		CK12 OCK1	System management	

TABLE 6. - AUXILIARY PROPELLANT KIT MEASUREMENTS REQUIRED FOR RCS FDA - Concluded

N T M T Z N				
Justification	System management	System management	System management	System management
Operating functional path	CK12 OCK1	CK13 0CK2	CK13 OCK2	CK13 0CK2
Soft limit Hard lim. t Correlation High low High low measurement				
lin. t low	TBD	ТВD	TBD	ТВD
Hard High	TBD	TBD	TBD	TBD
oft limit igh low	TBD	ТВD	TBD	ТВD
Soft High	TBD	х твр	X TBD	TBD
*⊃ v ə	<u>×</u>	×	×	×
Measurement	V43T0076A OMS fuel tank No 3 bulk temp - aux	V43T0274A OMS-OX tank No 1 bulk temp - aux	V43T0275A OMS-OX tank No 2 bulk temp - aux	V43T0276A OMS-OX tank No 3 bulk temp - aux

# 10.0 FLIGHT CONTROL SYSTEM/REACTION CONTROL SYSTEM INTERFACES

The interface between the flight control system (FCS) and the reaction control system (RCS) is not fully defined. The basic FCS/RCS interface is shown in figure 19.

### 10.1 Interface Operation

Redundant ON commands from the guidance and control computer are routed through two flight critical MDM's to the reaction jet driver input buffer. Loss of either ON command to the input buffer, or either command failed on, results in an illegal command signal to the computer. The failed jet is then removed from the jet select logic.

A valid ON command turns on the switching amplifier which applies +28 VDC to the .ue' solenoid valve coils, that open the engine inlet valves. The propellants then impinge and ignite in the thrust chamber. As chamber pressure builds up, the chamber pressure switches close sending a signal back to the monitor to indicate a good fire sequence.

### 10.2 Detectable Failure

Failure of one of the ON commands in either state results in an illegal command signal to the computer.

A legal ON command without a pressure switch closure results in a no-fire signal to the computer. In either case, the computer removes the thruster from the jet select logic.

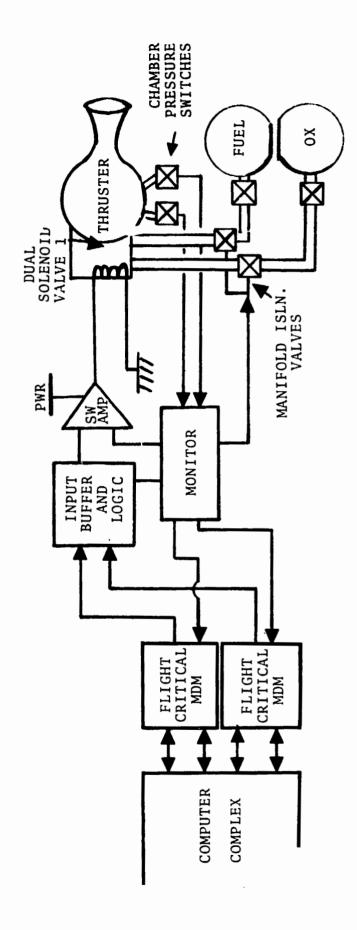


Figure 19. - Basic FCS/RCS interface.

A thrust chamber pressure switch closure without a valid ON command results in a failed on signal. The monitor closes the manifold isolation valves and the computer removes all jets on the manifold from the jet select logic.

#### 10.3 Undetectable Failures

except as a failed on jet. This failure presently results in the loss of all jets on the manifold. The addition of a switching amplifier output measurement and a circuit breaker, between the bus line and the amplifier, would allow single jet isolation for a switching amplifier on failure. Other methods to preclude a pressure switch failure from failing the whole manifold are being studied.

Failure of a single thruster inlet valve in the open position can only be detected as a leak. Addition of position indicators on the thruster inlet valves would eliminate this problem. The addition of manifold pressure measurements downstream of the thruster isolation valves is required, if the leak isolation method is used to isolate this failure.

#### 11.0 CONCLUSIONS AND RECOMMENDATIONS

### 11.1 System Definition

The RCS is not fully defined at this time; however, the basic measurement requirements for fault detection and annunciation should be nearly identical to those listed in this document.

#### 11.2 Forward RCS

Twenty-eight new measurements not presently included in the Master Measurement List, dated November 16, 1973, have been identified as requirements for FDA. These measurements should be added to the Master Measurement List.

The new measurements are identified as follows:

•	Engine	burn	through	monitors	16	ea
_						

• Manifold pressures 10 ea

• Helium source pressure 2 ea

Due to lack of configuration information on the forward RCS doors, monitoring of the RCS doors has not been considered in this report. Door monitoring will be required during operational missions.

### 11.3 Left and Right Aft RCS

Seventy-two new measurements not presently included in the Master Measurement List, dated November 16, 1973, have been identified as requirements for FDA. These measurements should be added to the Master Measurement List. The new measurements are identified as follows:

•	Engine burn through monitors	28 ea
•	Manifold pressures	20 ea
•	Manifold and tank SOV's	16 ea
•	Helium source pressures	4 ea
•	Engine temperatures	4 ea
	11.4 RCS Crossfeed/Interconnect	Operation

Eleven new measurements are required for crossfeed monitoring. They are identified as follows:

•	OMS crossfeed SOV position	4 ea
•	OMS helium source pressure	2 ea
•	Auxiliary propellant helium source pressure	l ea
		•

- Auxiliary propellant tank pressures 2 ea
- Auxiliary propellant SOV positions 2 ea

The RCS crossfeed valves are single point failures, which could result in depleting the RCS propellant tank associated with the failed valve during some OMS engine burns.

The RCS propellant tanks operate at a higher pressure than the cargo bay tanks. If the OMS engine is being supplied by the cargo bay propellant tanks, and an RCS crossfeed valve fails open, the associated RCS tank will be depleted. A study is being conducted by Rockwell International to resolve this problem. Consideration is being given to equalizing OMS and RCS ullage pressures.

### 11.5 FCS/RCS Interface

Consideration should be given to the following in the design of the reaction jet drivers.

As a minimum, the reaction jet drivers should provide the following:

- Redundant chamber pressure sensors.
- Jet driver output monitors.
- Jet driver electrical-ON failure isolation capability.
- Single jet driver power isolation capability.
- Failure identification annunciation.

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